ROUTE 67 (BANK STREET) SPOT IMPROVEMENTS

PRELIMINARY ENGINEERING REPORT

SEYMOUR, CONNECTICUT

State Project No. 124-165

MMI #3211-02-4

February 19, 2014 (Revised March 2016 to include Public Involvement Program)

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1.0 <u>Introduction</u>

In 1991, a study by Vanasse, Hangen, Brustlin, Inc. (VHB) assessed traffic conditions along the Route 67 corridor through Southbury, Oxford, and Seymour, Connecticut. In 2011, the Valley Council of Governments (VCOG) hired Milone & MacBroom, Inc. (MMI) to expand upon the 1991 report and to conduct operational analyses to further assess the impacts and validate or refine the earlier recommendations made by VHB. MMI's scope was limited to the segment of Route 67 in Seymour from Klarides Village, a retail development, to the River Street/Franklin Street intersection.

For this segment, VHB's initial recommendations included some mainline widening as well as spot improvements at various intersections including traffic signal retiming, redirection of side street traffic, realignment of side street(s), a roadway closure, and driveway access management. The improvements proposed by VHB are summarized as follows:

- Terminate Johnson Street at Route 67
- Prohibit left turns from Klarides Village by constructing a modified driveway median
- Revise the easterly segment of Old Drive to one way northbound
- Signalize the westerly intersection of Old Drive at Route 67
- Realign the Beecher Street/Church Street intersection with Route 67 for improved traffic operations
- Widen Route 67 between Franklin Street and Old Drive to extend the dual westbound travel lanes beyond 100 Bank Street

2.0 Purpose

The purpose of this study is to evaluate and provide a palette of roadway and intersection enhancements along the CT Route 67 (Bank Street) corridor between River Street/Franklin Street and Klarides Village to the west in the town of Seymour, Connecticut. This study provides an updated analysis to determine the current validity of the aforementioned improvements. Since



the VHB report and prior to MMI's analysis, a Walgreens pharmacy store was constructed east of Old Drive on the northern side of Bank Street. As part of its site plan approval, a new traffic signal was installed at its entrance drive, and two of the earlier VHB recommendations were essentially implemented. These recommendations include an additional traffic signal at the westerly intersection of Old Drive and modification of the easterly segment of Old Drive to a one-way northbound road.

A traffic study was conducted to analyze VHB's recommendations to determine whether current conditions warrant additional improvements. Six major intersections along the Route 67 corridor were analyzed. Of the six locations, it was determined that the three intersections below require geometric improvements while other areas benefit most by enhancing the existing traffic signal operations:

- Bank Street @ Franklin Street/River Street
- Bank Street @ Beecher Street/Church Street
- Bank Street @ Klarides Village/Johnson Street

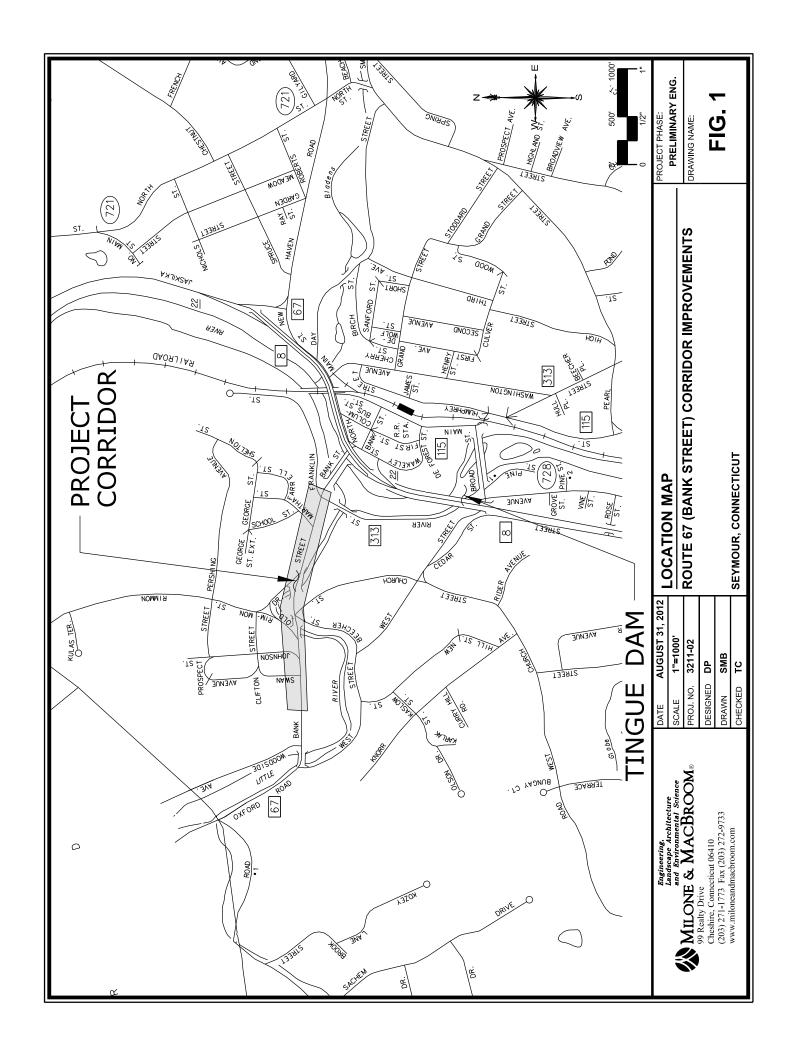
This preliminary engineering report summarizes existing conditions, discusses the overall corridor issues and opportunities, outlines the right-of-way and regulatory permit implications, and summarizes the traffic and pedestrian network analyses conducted by MMI. The assessment specifically identifies the three main locations where physical improvements are recommended and summarizes the benefits and impacts of each improvement along with a description of the alternatives considered. Figure 1 identifies the study area.

3.0 Existing Conditions

3.1 Corridor Characteristics

The section of Route 67 (Bank Street) that falls within the study area (between River Street/Franklin Street and the westerly end of Klarides Village to the west) is approximately one-third of a mile. Bank Street generally runs in an east/west direction through the western part of





town and provides connections to the town center area (via the Naugatuck River bridge) and to Oxford and points west. CT Route 8, which is elevated above the downtown area, provides regional access throughout the Naugatuck Valley region of Connecticut.

Within the study area, Bank Street generally has a single travel lane in each direction with auxiliary turn lanes at various intersections. While discontinuous at some locations, sidewalks are present along most of the project roadways, and the posted speed limit along Bank Street is 30 miles per hour (mph). The land uses through this corridor include retail, office, residential, and light industrial with most of the study area within the C-2 General Commercial Zoning District. At the eastern end of the project area, the zoning begins to transition to the CBD-1 Downtown Central Commercial District. A small area of residential zoning (R-18) abuts Route 67 at the Beecher Street/Church Street intersection. In addition, the C-2 and CBD-1 districts define the limits of the Enterprise Corridor Zone, which provides significant state and local tax incentives for new and existing businesses.

3.2 Parking

As indicated in the 2012 Seymour Master Economic Development Plan (MEDP), which was promoted as a "Downtown Action Strategy," the availability of both on-street and off-street parking was highlighted as a critical element to improving the downtown Seymour experience. On-street parking exists through the downtown area including areas along Bank Street that serve the adjacent retail establishments. As outlined later in this report, any geometric and operational improvements along the corridor need to be reviewed in relation to current and future demand for on- and off-street parking needed to support the adjacent land uses and future redevelopment initiatives. Within the study limits, two on-street parking spaces are currently provided on the north side of Bank Street (near Franklin Street) in front of the businesses at 80 and 82-84 Bank Street. On the south side of Bank Street, a wide shoulder supports "10-minute" on-street parking in front of the properties at 111-113, 115, and 117-119 Bank Street, which are immediately adjacent to the Little River and currently have no on-site parking. The remaining parking areas along the corridor are provided within off-street parking facilities.



3.3 <u>Regulatory Areas</u>

As shown on Figure 1, the Route 67 (Bank Street) project corridor is located immediately west of the Naugatuck River. At two locations within the study area, the Little River is conveyed under Bank Street. From west to east, the river then flows parallel to and behind the buildings along the southern side of Bank Street and eventually under River Street (CT Route 313) to its confluence with the Naugatuck River. As a tributary of the Naugatuck River, the Little River was studied in detail by the Federal Emergency Management Agency (FEMA), and specific floodplain elevations and floodway boundaries were established as shown on the most current FEMA Digital Flood Insurance Rate Maps (FIRMs) for Seymour. Since floodway and floodplain limits are shown across portions of the existing roads, each spot improvement within the corridor will need to be assessed in relation to the potential regulatory permit requirements including but not limited to the Connecticut Department of Energy & Environmental Protection (CT DEEP) Floodplain Management Certification.

In addition to the FEMA regulatory boundaries, field identification and delineation of Connecticut inland wetlands and federal wetlands within the project limits were performed. The wetland limits closely follow the floodplain boundaries and step banks associated with the rivers. Regulated activities associated with the wetlands, watercourses, and the related upland areas may require local, state, or federal permit approvals.

3.4 Historic and Archeological Significance

Within the project limits, there is one property that is eligible for the Register of National Historic Places. Provided within the Appendix of this report are copies of the correspondence between MMI and the Connecticut State Historic Preservation Office regarding 100 Bank Street. The design and construction of the improvements outlined within this report may need to be conducted in accordance with Section 106 under the National Historic Preservation Act.



3.5 <u>Drainage and Utility Infrastructure</u>

Using the Connecticut Department of Transportation (CTDOT) topographic survey as a basis for our investigations, supplemental topographic survey and field reconnaissance were performed to confirm existing flow patterns and assess the existing drainage systems. As the design of the preferred alternatives is advanced, the existing utility infrastructure will be reviewed again in relation to the proposed improvements in order to identify potential conflicts, required upgrades, and/or relocations. In addition, the existing utility infrastructure should be assessed in conjunction with any plans for redevelopment of the adjacent properties to identify and provide the necessary service laterals and prevent future disturbance of the completed improvements identified within this report.

3.6 <u>Abutting Property Owners/Project Stakeholders</u>

As indicated previously in this report, the project corridor includes a mixture of retail, office, residential, and light industrial land uses. Rights-of-way impacts to private property owners are discussed in more detail under various portions of this report. A summary of the property owners (now or formerly) within the study area based upon the Town of Seymour GIS Assessor records can be found in the Appendix of this report.

3.7 Traffic Operations

In order to validate and expand upon previous recommendations using current network conditions, a traffic analysis was performed along Route 67 (Bank Street). The following six intersections were studied:

- Bank Street @ Franklin Street/River Street (CT Route 313)
- Bank Street @ Old Drive (east)
- Bank Street @ Church Street/Beecher Street
- Bank Street @ Old Drive (west)



- Bank Street @ Klarides Village Driveway/Johnson Street (unsignalized)
- Bank Street @ Klarides Village (signalized)

The CTDOT records average daily traffic (ADT) volumes along state-owned highways. The ADT along Route 67, west of River Street and Franklin Street, was 20,000 vehicles per day (vpd) in the year 2009. Previous counts yielded 20,100 vpd in the year 2006 and 20,600 in the year 2003. According to the CTDOT, the average eastbound travel speed is 34 mph, and westbound speed is 35 mph. The 85th percentile speeds along Bank Street are 36 mph for eastbound travel and 38 mph for westbound travel. Manual turning movement traffic counts were collected on Thursday, May 5, and Thursday, June 9, 2011 during the morning and afternoon commuter peak periods (7:00 a.m. to 9:00 a.m. and 4:00 p.m. to 6:00 p.m.). The peak hours for the corridor are 8:00 a.m. to 9:00 a.m. and 5:00 p.m. to 6:00 p.m. Bank Street carries between 1,070 and 1,350 vehicles during the morning peak hour depending on the specific location. During the afternoon peak hour, 1,470 to 2,030 vehicles were counted. The manual counts collected vehicle classification data in addition to the traffic volume data. The analysis found that a greater percentage and overall number of heavy vehicles are present during the morning peak hour (1.5%) as opposed to the afternoon (.4%).

3.8 Accident Patterns

Using CTDOT accident records from January 2006 through December 31, 2008, an analysis of the accident history along the corridor was performed. There were 79 observed crashes. Of these crashes, 63 resulted in property damage only while 16 resulted in personal injury. The crashes resulted from a variety of collision types: rear-end, fixed object, sideswipe, intersecting turns, and same-direction turns. The most prevalent crash type was rear-end, which is typical for signalized intersections. A summary of the accident data is provided in Table 1.



TABLE 1 Accident Summary

		CCIDE EVERI		TYPE OF COLLISION								
					TURN							
LOCATION	INJURY	PROPERTY DAMAGE	LOTAL	INTERSECTING	SAME TURN	OPPOSITE	REAR-END	ANGLE	SIDESWIPE (Same Direction)	FIXED OBJECT	OTHER	TOTAL
		BAN	K STR	EET								
At Klarides Village Drive	5	17	22	4	1	2	13		1	1		22
Between Old Drive (west) and Klarides Village		2	2		1		1					2
At Old Drive (west)	4	2	6	4			1			1		6
Between Church Street and Old Drive (west)			0									0
At Church Street/Beecher Street	1	1	2			1	1					2
Between Church Street/Beecher Street and Old Drive (east)			0									0
At Old Drive (east)		7	7	4			3					7
Between Franklin Street and Old Drive (east)	3	14	17	4			4		5		4	17
At Franklin Street/River Street	3	20	23		2	4	11	1	3		2	23
TOTAL	16	63	79	16	4	7	34	1	9	2	6	79

Source: CTDOT 1/1/2006 to 12/31/2008

Crashes listed as "Other" at the intersection of Bank Street/River Street/Franklin Street and to the west of this intersection involved four incidents related to parking maneuvers in front of the retail shops. One related to a backing maneuver at the same location, and another involved a pedestrian conflict. The "Sideswipe" accidents in this location were primarily due to the short merge for westbound traffic just west of the intersection.

4.0 Future Traffic Conditions

4.1 Traffic Volumes

Future traffic volumes were forecasted using ambient traffic growth and site-specific traffic generated by proposed or future developments. Review of historic traffic count data for the area revealed an annual traffic growth factor of approximately 1%. Additionally, the CTDOT Bureau of Policy & Planning was contacted regarding this topic, and a 20-year horizon was mandated for purposes of analysis. CTDOT indicated a growth factor of 20% should be used to increase the existing 2011 traffic volumes to 2031.

4.2 Analyses

The corridor was modeled using *Synchro, Version 7*, a traffic operational modeling software package, for three scenarios: existing (2011) conditions, future (2031) no-build conditions, and future (2031) with improved conditions. The existing lane arrangements, signal timings, and phasing sequences were studied to identify existing deficiencies and opportunities. A Level of Service (LOS) was determined. The LOS is a qualitative measure of the efficiency of operations of intersections in terms of delay and inconvenience to motorists and is displayed with letter designations A through F. Summaries of the LOS and queues by approach for the existing traffic volumes are shown in Tables 2 and 3 for signalized and unsignalized intersections, respectively. The 2031 future background (no build) analyses results are summarized in Tables 4 and 5. The results of the 2031 future analyses incorporating the recommend improvements are provided under Section 7.0 of this report in Tables 9, 10, and 11.



TABLE 2 2011 Existing Traffic Volumes Level of Service Summary Signalized Intersections

	LEVEL OF SERVICE					
	WEEKDAY PEAK	MORNING HOUR		AFTERNOON HOUR		
APPROACH	LOS	QUEUE ^a	LOS	QUEUE		
Bank Si	reet/River Street/Franklin Street					
Eastbound (Bank Street)	A	89	В	252		
Westbound left/through (Bank Street)	С	155	Е	358		
Westbound right (Bank Street)	В	44	C	135		
Northbound left (River Street)	С	86	C	197		
Northbound through/right (River Street)	С	35	D	117		
Southbound left (Franklin Street)	С	55	C	113		
Southbound through (Franklin Street)	D	31	D	54		
Southbound right (Franklin Street)	В	33	В	130		
Overall	В		C			
Ва	ank Street/Old D	rive (west)				
Eastbound left (Bank Street)	A	4	A	19		
Eastbound through (Bank Street)	A	117	A	410		
Westbound (Bank Street)	В	103	С	958		
Southbound (Old Drive)	D	89	D	96		
Overall	A		С			
Bank Stre	et/Klarides Villa	ge Main Drivew	ay			
Eastbound (Bank Street)	A	226	С	689		
Westbound left (Bank Street)	A	9	A	6		
Westbound through (Bank Street)	A	77	A	217		
Northbound left (plaza driveway)	D	46	D	89		
Northbound right (plaza driveway)	В	26	В	34		
Overall	A		В			

^a 95th percentile queue in feet

TABLE 3 2011 Existing Traffic Volumes Level of Service Summary Unsignalized Intersections

	LEVEL OF SERVICE					
		MORNING HOUR		AFTERNOON HOUR		
APPROACH	LOS	QUEUE ^a	LOS	QUEUE		
Bank Street/Old Drive (east)						
Eastbound left (Bank Street)	A	0	В	0		
Bank Street/Church Street/Beecher Street						
Westbound left (Bank Street)	A	7	В	18		
Northbound (Church Street)	С	29	F	77		
Bank Street/Klarides Village unsignalized driveway						
Westbound (Bank Street)	A	7	A	19		
Northbound (plaza driveway)	В	19	С	41		

^a 95th percentile queue in feet

TABLE 4 2031 Future Background Traffic Volumes (No Build) Level of Service Summary Signalized Intersections

	LEVEL OF SERVICE						
	WEEKDAY PEAK	MORNING HOUR		AFTERNOON HOUR			
APPROACH	LOS	QUEUE ^a	LOS	QUEUE			
Bank Si	treet/River Street	reet/River Street/Franklin Street					
Eastbound (Bank Street)	A	146	С	326			
Westbound left/through (Bank Street)	С	190	F	465			
Westbound right (Bank Street)	В	53	С	166			
Northbound left (River Street)	С	102	С	259			
Northbound through/right (River Street)	С	40	D	141			
Southbound left (Franklin Street)	С	63	С	135			
Southbound through (Franklin Street)	D	36	С	65			
Southbound right (Franklin Street)	В	39	С	154			
Overall	В		Е				
Bo	ank Street/Old D	rive (west)					
Eastbound left (Bank Street)	A	5	A	18			
Eastbound through (Bank Street)	A	185	В	479			
Westbound (Bank Street)	В	173	F	1083			
Southbound (Old Drive)	D	100	D	111			
Overall	A		F				
Bank Stre	et/Klarides Villa	ge Main Drivew	yay				
Eastbound (Bank Street)	A	376	D	859			
Westbound left (Bank Street)	A	7	A	5			
Westbound through (Bank Street)	A	281	В	182			
Northbound left (plaza driveway)	D	253	D	91			
Northbound right (plaza driveway)	В	27	В	35			
Overall	A		С				

^a 95th percentile queue in feet

TABLE 5 2031 Future Background Traffic Volumes (No Build) Level of Service Summary Unsignalized Intersections

	LEVEL OF SERVICE						
	WEEKDAY PEAK	MORNING HOUR		AFTERNOON HOUR			
APPROACH	LOS	QUEUE ^a	LOS	QUEUE			
В	Bank Street/Old Drive (east)						
Eastbound left (Bank Street)	A	1 C		2			
Bank Sti	t						
Westbound left (Bank Street)	В	11	В	30			
Northbound (Church Street)	D	55	F	205			
Bank Street/Klarides Village unsignalized driveway							
Westbound (Bank Street)	A	8	A	24			
Northbound (plaza driveway)	C	25	С	50			

^a 95th percentile queue in feet

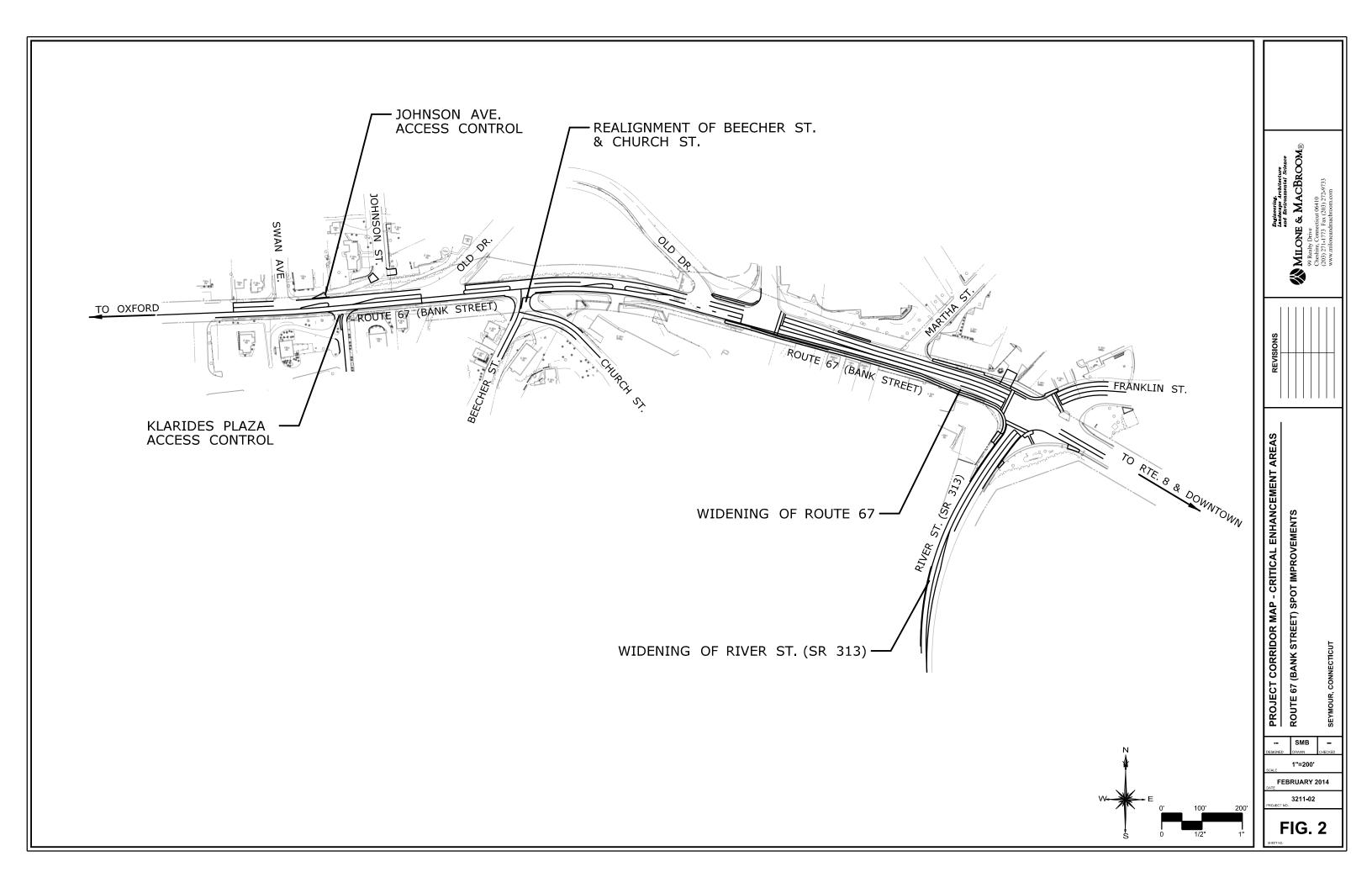
The decreases in LOS identified above highlight those locations within the corridor that would benefit from geometric and/or operational improvements. Review of these results allowed MMI to identify deficiencies, test the benefits of certain improvements, and investigate design alternatives detailed herein.

5.0 Proposed Improvements

The traffic analyses performed in relation to the existing and future traffic conditions confirm the original findings presented by VHB. Since VHB's earlier report, some of the recommendations have been implemented through completed development projects immediately adjacent to Bank Street. While these spot improvements have provided isolated operational improvements, additional geometric and system enhancements should be pursued and assessed along the corridor as a whole.

The following three improvement locations as shown in Figure 2 are highlighted as critical enhancement areas along with some operational improvements at two signalized intersections:





- Bank Street @ Franklin Street/River Street and @ Old Drive
- Bank Street @ Beecher Street/Church Street
- Bank Street @ Klarides Village/Johnson Street

5.1 Route 67 (Bank Street) from Old Drive to Franklin Street/River Street (SR 313)

In 1991, VHB recommendations included widening Route 67 between the Franklin Street/River Street intersection and the Old Drive intersection to accommodate an additional westbound travel lane. Also, VHB proposed turning the easterly segment of Old Drive into a one-way northbound road and installing a signal at the intersection of Bank Street and Old Drive West. As noted earlier in this report, a Walgreens Pharmacy was built east of the Old Drive intersection. As part of its local land use approval and consistent with the 1991 recommendation, a signal was installed at the westerly intersection of Old Drive, and the easterly segment of Old Drive was improved to a one-way northbound road.

The Old Drive East intersection is an unsignalized intersection adjacent to the intersection with the signalized Walgreens driveway at Bank Street. Since these two intersections are in close proximity (approximately 150 feet), the signal has a direct effect on the operations at Old Drive. Bank Street has a single westbound lane and one eastbound through lane although the left-turn lane from the Walgreens driveway does provide queuing for approximately two vehicles entering Old Drive. A sidewalk is located along the southern side of Bank Street and at the northeast corner of the intersection. A path exists along the western side of Old Drive. While there are pedestrian ramps on both sides of Old Drive, there is no marked crossing for the northern leg of this intersection. Crosswalks do exist at the Walgreens driveway intersection, with pedestrian push buttons for signalized assistance concurrent with the side street green phase.

The additional westbound Bank Street travel lane discussed above and supported in this study is intended to alleviate queuing issues approaching the Walgreens and Old Drive East intersections and improve the flow of traffic through this intersection. Currently, those traveling west along

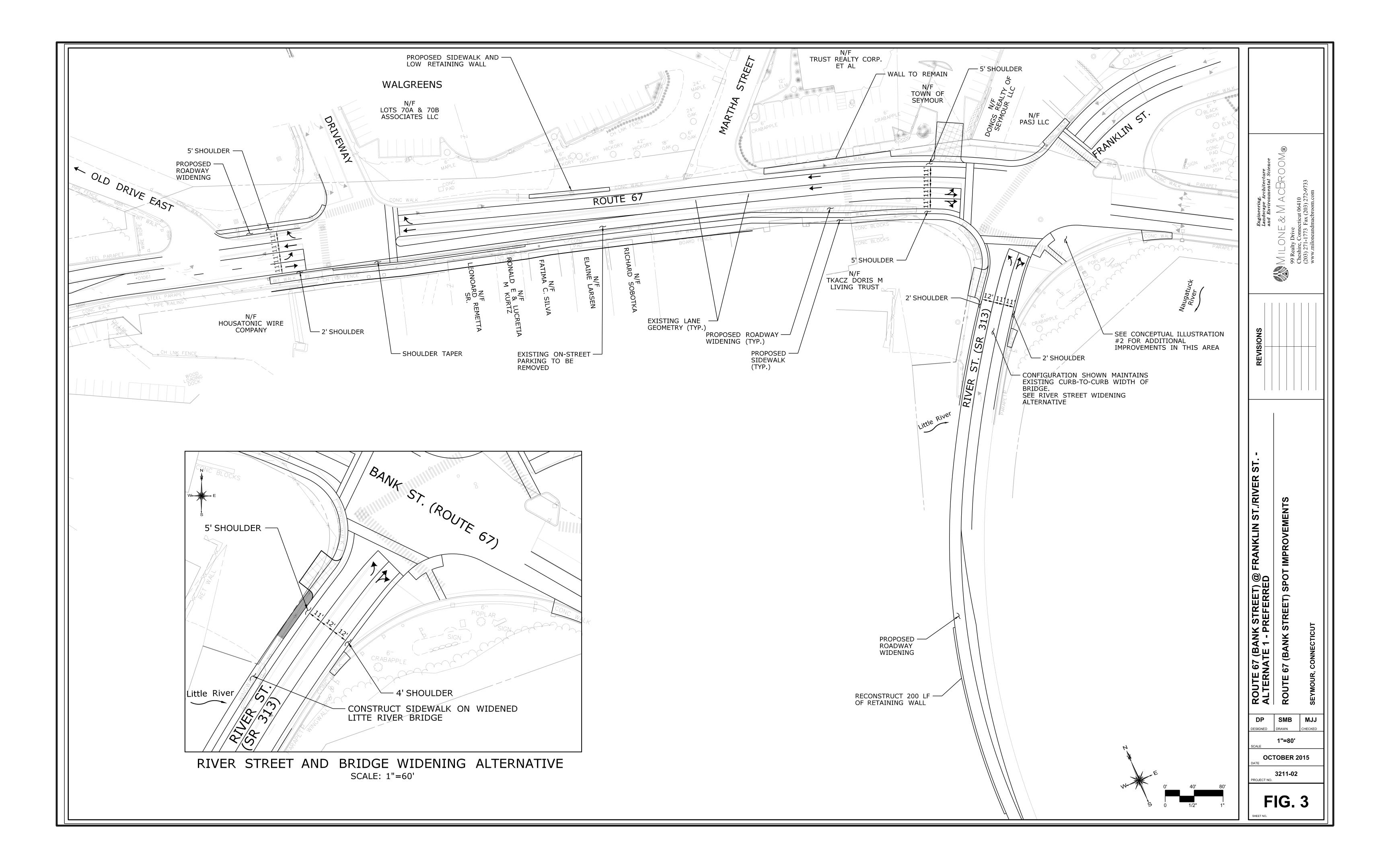


Bank Street are required to merge to a single lane only 200 feet west of the Franklin Street/River Street intersection and just before the Martha Street intersection in order to cross the bridge just west of the Old Drive East intersection. Widening of the road will allow queuing in the right-turn lane at the Walgreens intersection and will extend the merge length for westbound vehicles. It was also determined that not only should Bank Street be widened between Franklin Street and Old Drive but operational improvements would be needed for the Bank Street/Franklin Street/River Street intersection along with redesign of the signal.

The Bank Street/Franklin Street/River Street intersection operates under signal control with Bank Street approaching from the east and west, Franklin Street serving as the northern leg, and River Street to the south. The westbound Bank Street approach has one shared left-turn/through lane and one shared through/right-turn lane with channelization for the right turns. The eastbound approach also has two general-purpose lanes. The northbound approach has an exclusive left-turn lane and a through/right-turn lane. The southbound approach has exclusive left-turn, through, and right-turn lanes. Crosswalks are present at the northern, southern, and western legs of this intersection. The signal phasing provides for an exclusive pedestrian phase, which is activated by push buttons at each corner. Sidewalks extend from all legs of this intersection.

Following our analysis and assessment of the conditions within the project corridor and discussions with the Town of Seymour and VCOG staff, it is recommended that the preferred design for this section of Route 67, referred to as Alternate No. 1 and shown in Figure 3, include widening (primarily) on the south side of Bank Street between Old Drive East and the Franklin Street/River Street intersection. Based upon input from the VCOG and Town of Seymour, earlier concepts now include the use of 11-foot lanes with 5-foot shoulders to support on-street bicycle connectivity from the areas adjacent to Bank Street to downtown Seymour and the developing riverfront recreational opportunities. Aside from the minor widening and the construction of a small retaining wall on the north side of Bank Street, immediately in front of Walgreens, the concept holds the northern edge of pavement and extends the widened pavement section to the south. In doing so, the new edge of pavement and sidewalk create direct impacts to the buildings along the southern side of Bank Street including but not limited to direct impacts



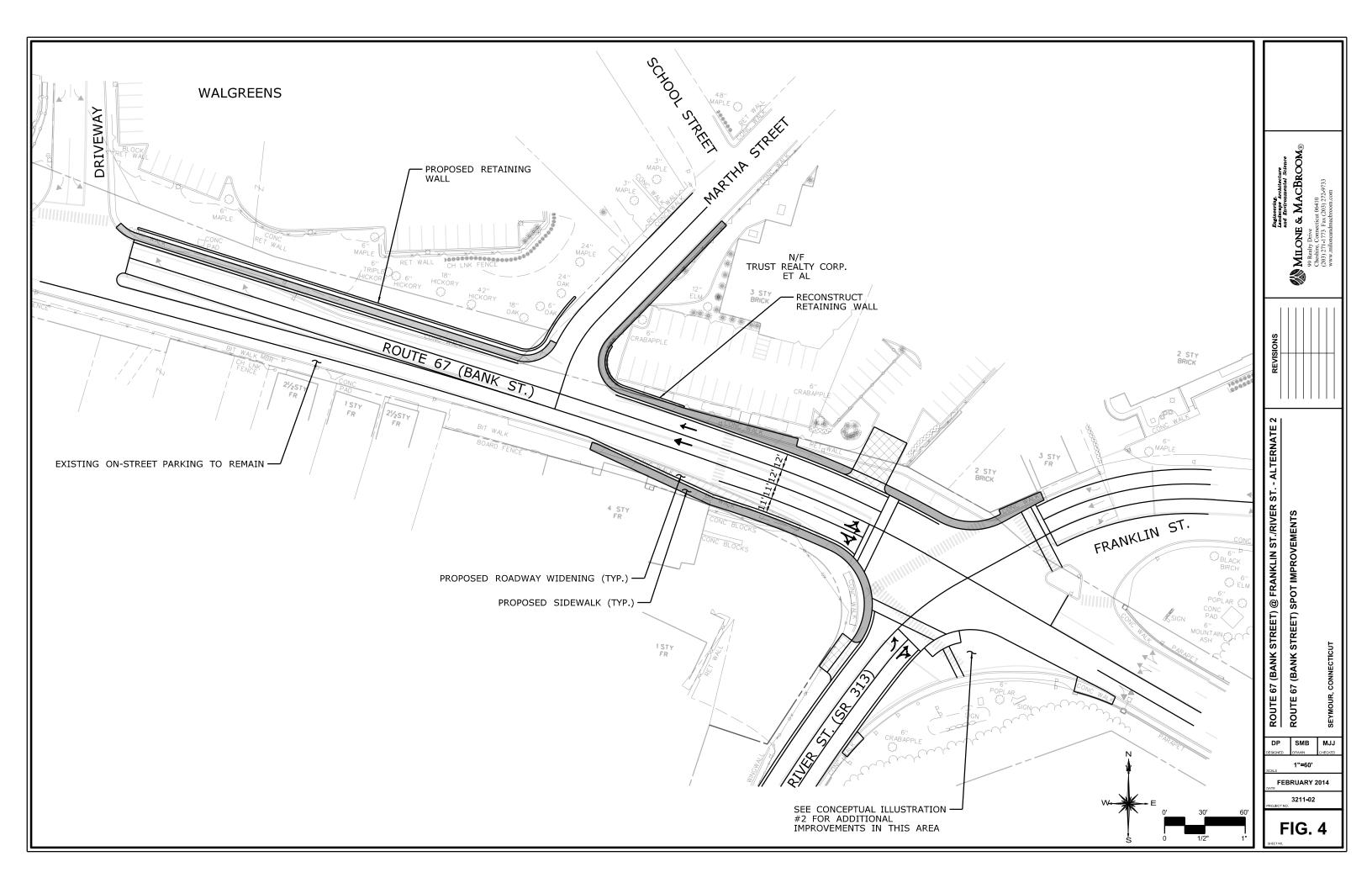


to the buildings and porches and the elimination of the limited "10-minute" on-street parking. In addition to the direct building impacts, the loss of parking constitutes a serious impact given the lack of on-site parking spaces and the current short-term on-street parking used by these properties and businesses. Given the loss of parking, acquisition of these properties may be necessary and therefore is assumed in the cost analysis. While the town supports the preservation and/or creation of on-street parking within the downtown area, the acquisition of such properties may provide opportunities to reshape the south side of Bank Street in this area to either establish new on-street parking beyond the widened lane arrangement or to create off-street parking as part of redevelopment efforts planned for the southwest corner of the Bank Street/Franklin Street/River Street intersection. These concepts will be explored further by the Town of Seymour and VCOG as the design of these spot improvements and the adjacent redevelopment area evolves.

The preferred alternate also extends the westbound right-turn lane at the Walgreens driveway through to the intersection of Old Drive East to accommodate the traffic volumes at this location and continue the intended pedestrian and on-street bicycle patterns through the corridor. The improvements at the entrance to Walgreens propose to shift the existing Bank Street crosswalk from the western to the east side of the intersection. The shift increases the distance between the existing crosswalk and the end of the Route 67 Little River bridge parapet and improves the sight distance and visibility associated with this existing pedestrian and potential future bicycle crossing.

An alternative to the preferred, Alternate No. 2, as shown in Figure 4, proposes to only widen the northerly side of the road. A large retaining wall would need to be built along the northerly side west of Martha Street in order to retain the slope. Also, to the east of Martha Street, the existing retaining wall at 100 Bank Street would have to be reconstructed and shifted north to accommodate the widening. While this retaining wall may provide an appealing and historic aesthetic along this section of Bank Street, large portions are in disrepair. Furthermore, removal of the wall may require assessment and proper documentation in accordance with Section 106 under the National Historic Preservation Act given that the property is eligible for listing on the





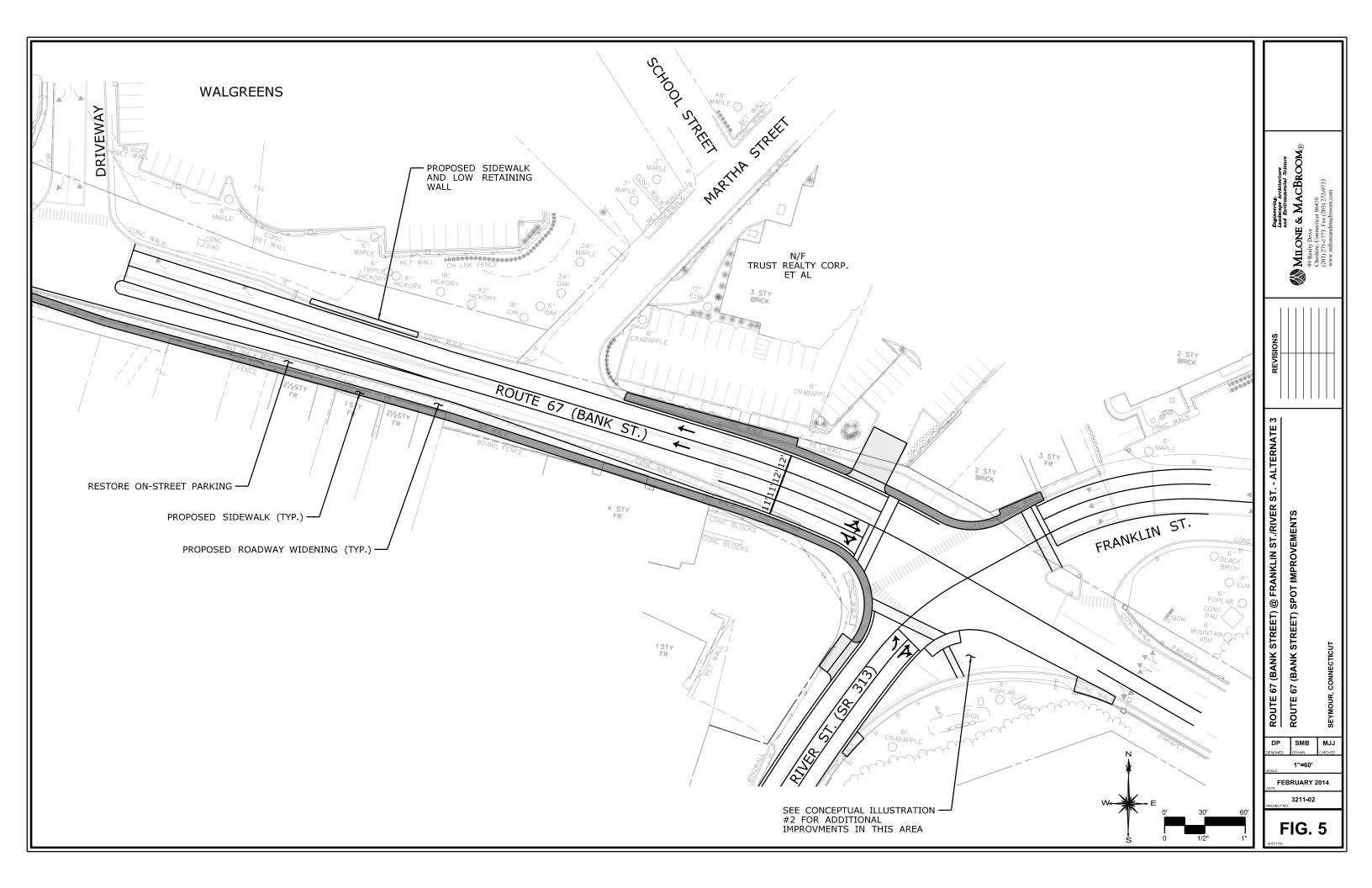
National Register of Historic Places. Widening to the north will also steepen the grade of Martha Street and impact the off-street parking at 100 Bank Street. For the reasons summarized above, this alternative has been deemed undesirable.

Alternate No. 3, proposing more extensive impacts (shown in Figure 5), was also considered. The concept is similar to the design approach shown in Figure 3 for Alternate No. 1 but preserves the on-street parking along the southern side of Bank Street. While the preferred alternative (Figure 3) may result in acquisitions due to the loss of parking, the design shown in Figure 5 will require full acquisition of several parcels to accommodate the widening and preservation of on-street parking. The alternatives shown in Figures 3 and 5 may need to be reviewed/considered together in relation to available funding and plans for redevelopment in the area.

The preferred option and the alternatives each require encroachment upon the existing sidewalk, building, and right-of-way along the south side of Bank Street and immediately west of the River Street intersection in order to maintain the current lane configurations. Also, both the preferred and alternative improvement options will require additional enhancements to the Franklin Street/River Street intersection including the removal of the two on-street parking spaces along Bank Street at the northwest corner of the intersection. The accident history indicates numerous crashes have occurred in this area due to parking maneuvers. A reduced curb-to-curb width at this location will shorten the crossing distance for pedestrians.

Furthermore, the curb radius for the River Street right-turn lane northbound movement at the southeast corner of the intersection may be reduced substantially. The existing radius exceeds 150 feet, which is more than adequate for trucks making right turns northbound onto Bank Street. A reduced radius would serve to slow vehicles making this turn, shorten the distance for pedestrian crossings, and provide additional landscape area and possible connections to the town's Naugatuck River recreational resources.





Modifying the signal timing to provide additional green time for the Bank Street east/west phase will also be needed to improve the LOS at this intersection. This is the phase with the heaviest traffic volumes. The increased time for this phase can be expected to improve the weekday afternoon overall operations from LOS E to LOS C, with little impact to northbound and southbound movements. The westbound approach will improve from LOS F to LOS C, and the 95th percentile queue at this approach can be reduced by over 140 feet.

As supported by the results from our traffic analysis, widening the northbound (River Street) approach to this intersection to extend the left-turn lane should also be pursued. The 95th percentile queue for this lane exceeds 300 feet. The widening of River Street to lengthen the northbound left-turn lane was assessed in conjunction with our review of the inspection reports for the River Street (SR 313) bride (No. 01585) over the Little River. While the bridge is listed as being constructed in 1936 (and reconstructed partially in 1991), it remains in fairly good condition as represented in the bridge inspection report. Currently, it supports the existing and proposed lane arrangement except for the continuation of the 5-foot (bike lane) shoulder from Bank Street to River Street. The structure's overall rating is adequate, but the curb-to-curb deck width does not meet the current requirements. The latest inspection report indicates the curb-tocurb distance is currently 37.5 feet, which is well below the minimum criteria, resulting in a deck geometry appraisal rating of 2. According to the Federal Highway Administration (FHWA) Recording and Coding Guide for the Structure Inventory and Appraisal of the Nation's Bridges, a rating of 2 is defined as "basically intolerable requiring high priority of replacement." Upon closer review, there are significant factors that would complicate the widening along eastern River Street including the proximity of the bridge to the Naugatuck River and the configuration of the wingwalls, which primarily run parallel to River Street. These factors limit the ability to widen the bridge superstructure, add a cantilevered section for sidewalk, etc. For the purposes of this study and in order to avoid regulatory obstacles associated with working within the Naugatuck River FEMA floodway, the widening of River Street and the River Street bridge is assumed to be along the western side of the road. In order to accommodate the widening of River Street, a new retaining wall will need to be constructed or the existing retaining wall reconstructed along the western side of the road in the area south of the former Housatonic Wire



Company property. The existing eastern edge of pavement would be maintained in its current location. The widening of River Street in this area will need to be reviewed concurrently with the town's parallel efforts to investigate and plan riverwalk extensions along the Naugatuck River and around the Tingue Dam recreational and park areas.

When assessed in conjunction with the improvements recommended herein, the capacity analysis detailed in the traffic study indicates that the LOS would improve at the intersection of Bank Street/Franklin Street/River Street, experiencing an overall operational improvement from LOS E to LOS C during the afternoon peak hour. This enhancement is primarily caused by the improvement to the westbound through traffic. By providing additional time for this movement, the operations will improve for this approach from LOS F to LOS C during the afternoon peak hour. The afternoon queues at this approach can also be reduced by approximately 220 feet, and the morning queues would also show improvement.

Table 6 below details a very early opinion of approximate construction costs of the alternates along this specific section of Route 67 expressed in 2014 dollars. A more comprehensive cost analysis that includes all of the improvements associated with the preferred alternates summarized herein can be found in the Appendix of this report.

TABLE 6
Bank Street Between Old Drive and
River Street/Franklin Street Intersection
(not including River Street widening)

	2014
Improvement	Cost*
Alternative 1 - preferred	\$1,029,000
Alternative 2	\$1,552,000
Alternative 3	\$1,270,000

^{*}Excludes right-of-way acquisition costs, utility relocations, streetscape enhancements, and hazardous materials, if any



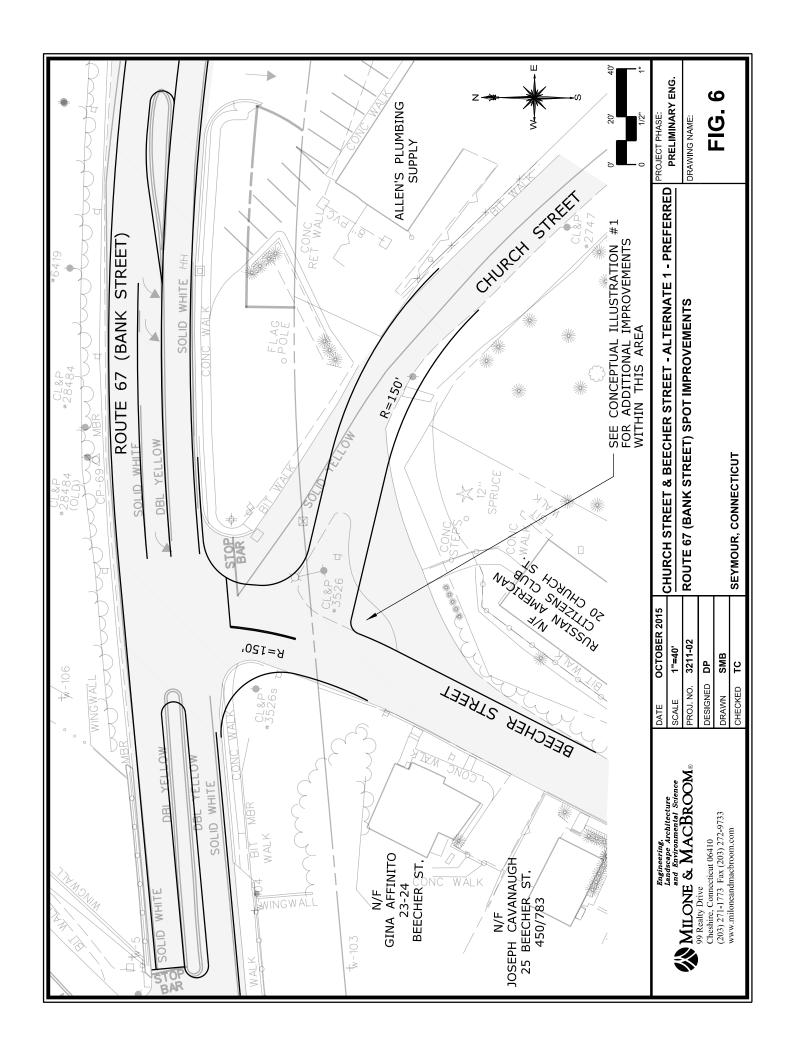
5.2 Bank Street @ Church Street/Beecher Street

Church Street approaches Bank Street from the southeast and carries two-way traffic while Beecher Street departs toward the southwest (away from Bank Street) as a one-way street. Bank Street provides a single eastbound lane. Westbound Route 67 has one through lane and an exclusive left-turn lane for motorists entering Church and Beecher Streets. The side streets operate under stop sign control, and there are no controls on the mainline (Route 67). A sidewalk exists along the southerly side of Bank Street; however, no crosswalks exist. The intersecting streets are skewed with a crossing distance of approximately 60 feet. Currently, the intersection is a safety concern with little vehicle priority established. With such a wide entrance, those traveling westbound along Bank Street and turning onto Beecher Street must contend with those traveling eastbound on Bank Street turning right onto Church Street. MMI agrees with VHB's original recommendation that this intersection be reconfigured to provide for safer traveling movements.

MMI initially considered reconfiguring Church and Beecher Streets such that Beecher Street forms the leg of a T-intersection with Church Street with two northbound approach lanes. In turn, Church Street would be narrowed/realigned at its intersection with Bank Street. This would provide a narrower intersection, reduce vehicular speeds and the potential for conflicts, and shorten the pedestrian crossing distance. However, upon review of site conditions and preliminary engineering efforts, a T-intersection along Beecher Street (instead of Church Street), along with the narrowing and realignment of the intersection at Bank Street, may be more feasible (shown in Figure 6). This figure represents Alternative No. 1.

This alternative will create a safer condition for both vehicular and pedestrian mobility, will result in the same overall improvement to traffic operations at a much lower cost, and will not require the acquisition of private property. This approach will reduce the width of the curb cut at Bank Street and create a T-intersection with Beecher Street and Church Street. Currently, there is an informal roadway/access strip for drop-off and pickup in front of the Russian American Citizen Club. This area is within the public right-of-way but is used almost exclusively by the





club. Under this option, the access strip will remain available for limited parking and, through the use of streetscape design elements, there is potential to enhance the overall appearance of these intersections and the drop-off area (see Conceptual Illustration #1). Options to narrow Beecher Street to allow for additional on-street parking along the Russian American Citizens Club frontage were also considered but, given the current on-street parking associated with the existing residences on the opposite side of the street, this was not incorporated into the preferred alternative.

The additional turning lane on Beecher Street approaching Bank Street will help to reduce delays for motorists turning right due to left-turning vehicles. Morning peak-hour queues will be reduced by approximately 40 feet and afternoon peak-hour queues by nearly 150 feet. The two-lane configuration will yield afternoon operations of LOS D for right-turning vehicles, which is an improvement from the LOS F condition experienced by the current single-lane approach.

The alternative to this improvement, Alternate No. 2, would be similar to the original VHB recommendations, which would create the primary intersection of Church Street at Bank Street with Beecher Street intersecting Church Street at 90 degrees. The impacts to traffic are similar; however, it was determined that geometrically creating a T-intersection along Church Street would be much more extensive and would require adding a significant amount of pavement and regrading. This option will also involve the acquisition of property to the east of the intersection and would eliminate the roadway strip in front of the Russian American Citizen Club. Figure 7 details this option.

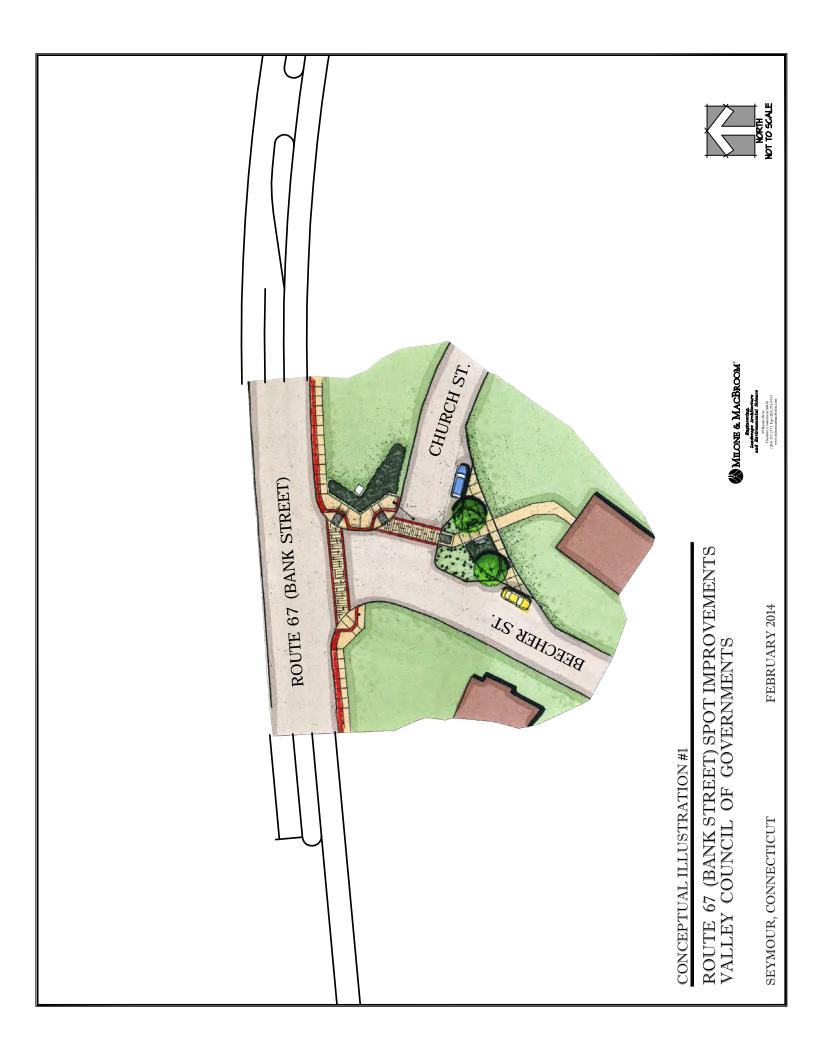
Table 7 below details the estimated costs per each improvement.

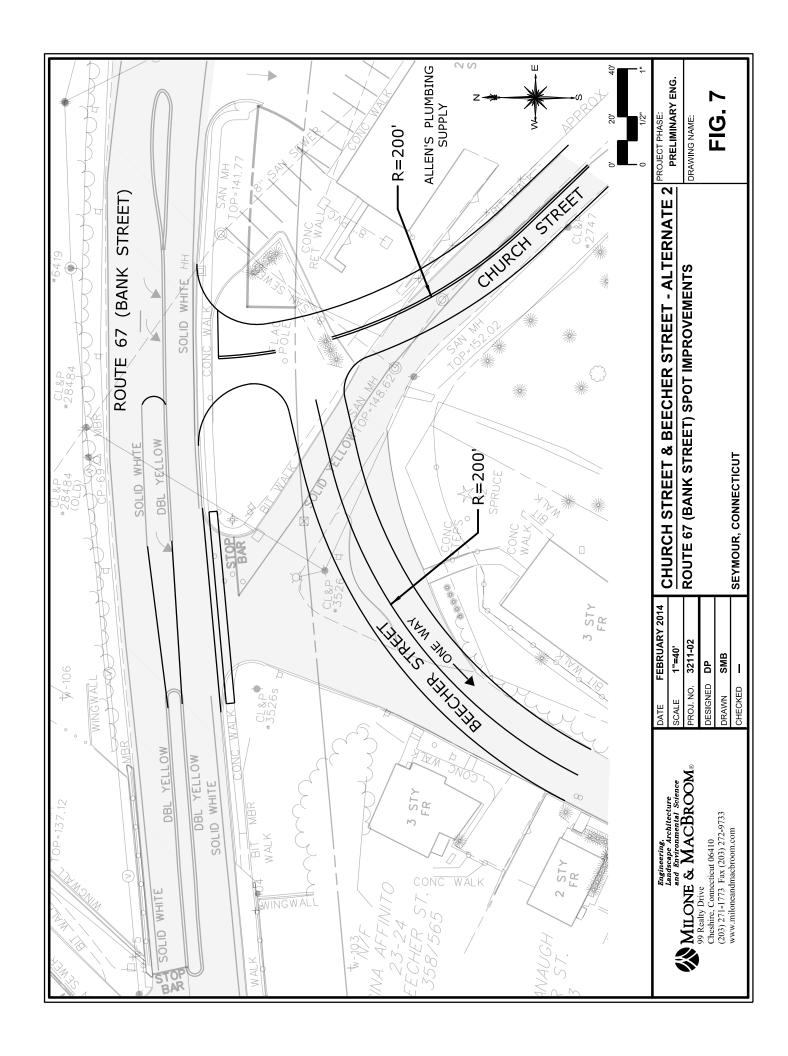
TABLE 7
Bank Street/Church Street/Beecher Street

Improvement	2014 Cost*
Alternative 1 - preferred	\$207,000
Alternative 2	\$470,000

^{*}Excludes right-of-way acquisition costs, utility relocations, streetscape enhancements, and hazardous materials, if any







5.3 Bank Street @ Klarides Village Driveway/Johnson Street

This intersection is located at the easterly end of Klarides Village, between the McDonald's restaurant and TD Banknorth. The plaza driveway has a single exit lane, which is signed to prohibit left turns onto Bank Street. Bank Street provides for a single lane in each direction at this location. Opposite the plaza driveway is a retaining wall that supports Johnson Street, a steep, one-way southbound roadway (toward Bank Street) with a left-turn prohibition. Johnson Street is sharply skewed with Bank Street. The angled approach (from the northeast) results in a poor sightline looking to the left when entering Bank Street. Johnson Street serves a residential neighborhood.

Currently, the intersection has a good LOS of A along the westbound approach on Bank Street during both AM and PM peak hours, a LOS of B at the northbound plaza driveway in the AM, and a LOS of C during the PM peak. Future conditions show a decrease in the AM northbound plaza drive approach to a LOS of C.

A sidewalk is present along the southern side of Bank Street, and the length of the pedestrian crossing at the plaza driveway is approximately 32 feet. There is no sidewalk on the northern side of Bank Street. The sidewalks to the east of the intersection and on the southerly side are in good condition; however, the grass strip at the edge of the road requires restoration. The sidewalk to the west, toward the signalized driveway, is in poor condition. The curb reveal is diminished, and there is need for curbing along an abandoned curb cut. Lastly, mulch eroded from the adjacent landscape bed is migrating onto the walkway.

The proposed improvements from the original study were to terminate Johnson Street at Route 67 along with prohibiting left turns from Klarides Village by constructing a modified median. MMI found these improvements to remain valid and has made the following recommendations and improvements.

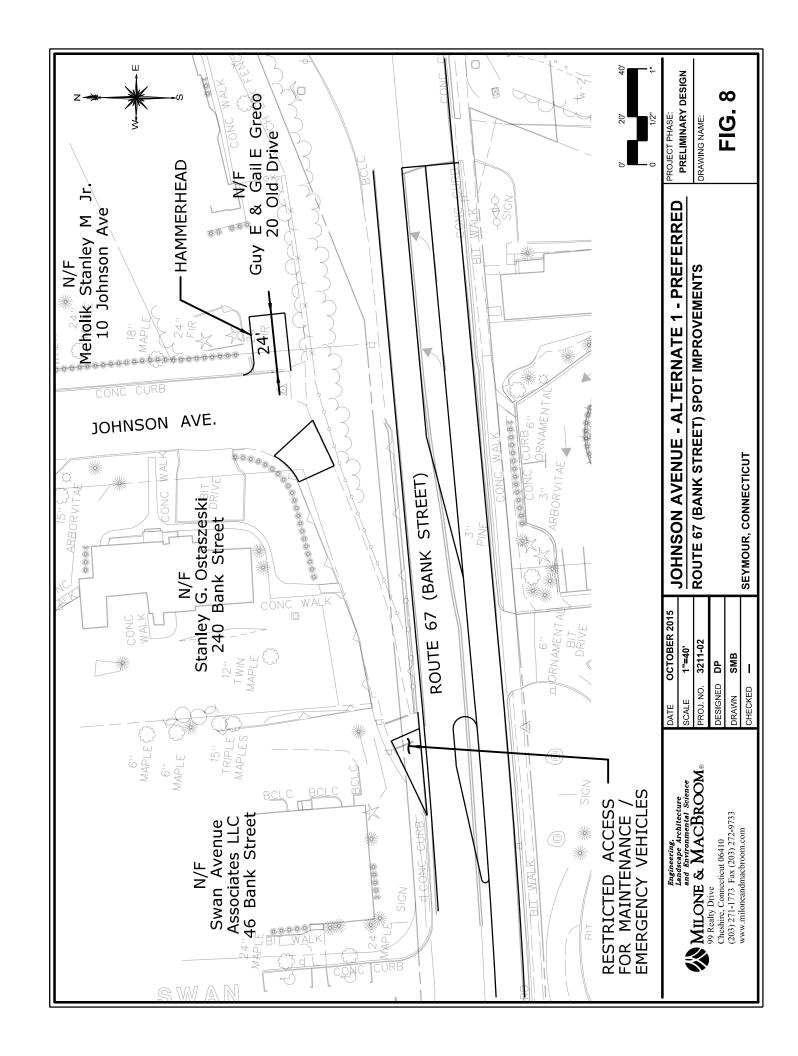


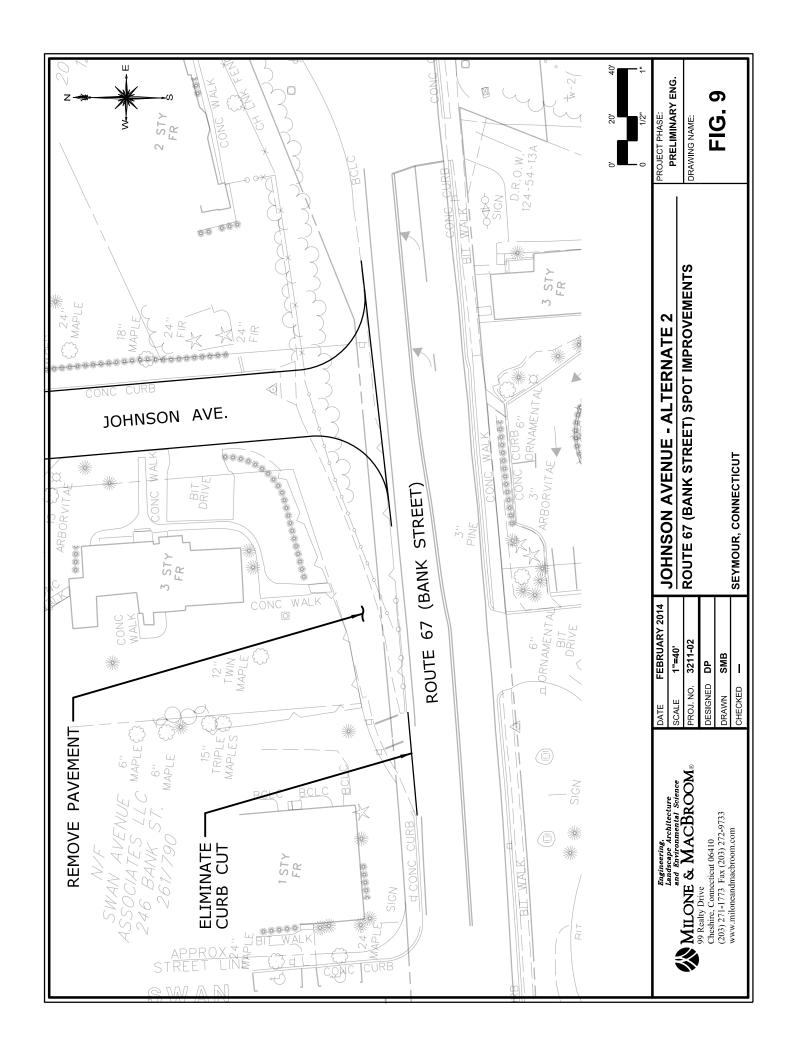
5.3.1 Johnson Street at Bank Street

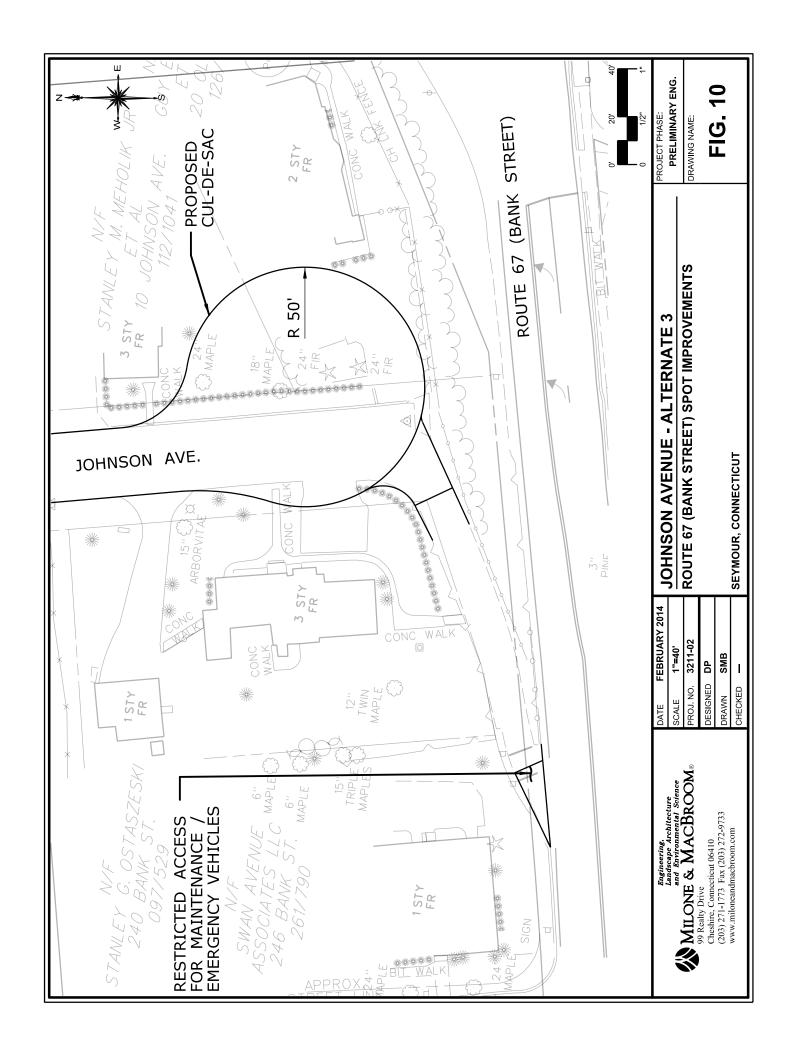
In order to improve safety associated with the sharply skewed intersection of Johnson Street and Route 67, closure of the southerly portion of Johnson Street to traffic while maintaining access only for emergency and maintenance vehicles should be pursued. Since Johnson Street will need to remain a two-way street, provisions for vehicles to turn around will be needed. Of the several options considered, the preferred alternative offered herein includes the construction of a hammerhead intersection immediately adjacent to the existing residential properties closest to Route 67 that would allow the access of emergency and maintenance vehicles. In order to deter drivers from using this access point, raised brick pavers and decorative landscaping are proposed to limit access. This plan will require a partial taking from the Mehalick residence to the east for the turnaround portion. Currently, the approach to Bank Street is dangerous and has poor sightlines. Elimination of this access point will improve the safety of users at this intersection and provide for a free flow of traffic along Route 67. However, this option will require Johnson Street area residents to seek alternate access to Route 67. Minor drainage adjustments may be needed to address runoff from the additional impervious area proposed. Figure 8 details the preferred Alternate No. 1.

Two additional road closure alternatives were considered. Alternate No. 2 shown in Figure 9 considers creating a T intersection with Route 67. However, the significant elevation difference of approximately 25 feet would require extensive filling and regrading along Johnson Street, which will also create access issues for some of the residential properties along the street. The roadway profile of Johnson Street is approximately 10%. A T-intersection construction would require a road profile in excess of 25%, which creates an unsafe condition and would exceed the maximum allowable grade per local regulations. The third alternative proposes creating a culde-sac at the end of Johnson Street. As shown in Figure 10, the cul-de-sac would terminate above the steep slope above Route 67 but would encroach on the Byrne residence to the west. Given the impacts to private properties, this alternative has been deemed undesirable.









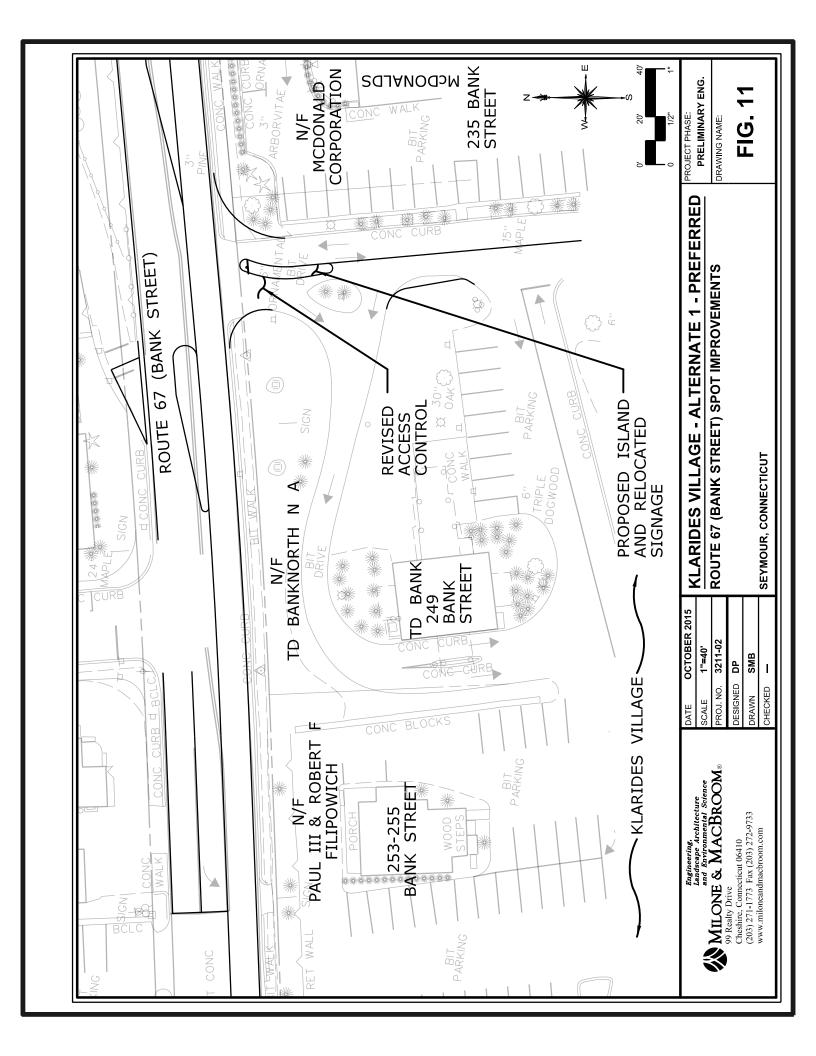
5.3.2 <u>Klarides Village and Bank Street (unsignalized)</u>

The second improvement recommended for this intersection was to better enforce the no-left-turn movement by adding a physical barrier. Currently, the left-turn is prohibited by a sign posted opposite the driveway; however, there is a tendency for drivers to turn left. As shown in Figure 11, the preferred alternative includes constructing a delta island within the driveway area to physically restrict and prohibit left turns.

This enhancement will reinforce the existing intersection design. The illegal left turns that are occurring create safety issues crossing Route 67 and block traffic attempting to exit right out of the Klarides driveway. Those turning left or heading east along Route 67 will be required to drive through the plaza to the existing signalized driveway. This allows for safer movements and provides better traffic flow along the corridor. Physically prohibiting the ability to turn left will eliminate the safety concerns and the queuing issues at the unsignalized intersection. This design will require the removal of the existing landscaped island in order to accommodate the new geometry of the landscaped raised median. In addition, the No Left Turn signage should be located on the new island for better visibility. This design is expected to have minimal to no impacts on rights-of-way and utilities. Stakeholder impacts will be essentially limited to those patrons exiting McDonald's and TD Banknorth and wishing to travel east on Route 67.

The second alternative explored would further restrict the movement of vehicles at this location. This alternative would make the driveway one way, permitting ingress only. This option would eliminate the option to exit eastbound and would require patrons to travel through the plaza to the signalized driveway. This option would also create more congestion at the signalized driveway and within the property and would further impact convenience. This alternative would also increase delays at the signalized driveway and possibly impact businesses adversely.





Overall, with the suggested improvements made at Johnston Street and the Klarides Village driveway, the goal to limit left turns will be achieved along with creating a safer flow of traffic by eliminating the Johnson Street entrance. While these improvements will not provide a significant change in the LOS C, they will provide for a safer driving experience.

Table 8 below details the estimated costs per each improvement.

TABLE 8
Bank Street @ Klarides Village/Johnson
Street

Improvement – Johnson Street	2014 Cost*
Alternative 1 – preferred	\$72,000
Alternative 2	\$1,126,000
Alternative 3	\$191,000
Alternative 4	\$261,000
Improvement – Plaza Driveway	
Alternative 1 – preferred	\$38,000
Alternative 2	\$31,000

^{*}Excludes right-of-way acquisition costs, utility relocations, streetscape enhancements, and hazardous materials, if any

6.0 Additional Traffic Signalization Improvements

Along with specific geometric improvements, signalization improvements are recommended at two intersections. These two intersections are described below.

6.1 <u>Klarides Village</u>

With the enhancements at the Klarides Village and Johnson Street intersection, signal improvements at the Klarides Village signalized driveway will also be needed. The plaza driveway approaches Bank Street from the south with two lanes, one left-turn lane and one right-turn lane. The eastbound Bank Street approach has a single lane while the westbound approach has an exclusive left-turn lane and a through lane. A sidewalk is present along the southern side



of Bank Street, and a crosswalk connects to two corners at the southeast and southwest. Another crosswalk is present across Bank Street at the western leg of the intersection. The walk phases operate concurrently with the corresponding green phases.

The traffic analysis supports modifying the signal timing at this intersection. Reducing the cycle length from 90 seconds to 60 seconds will maintain overall operations of LOS A and will significantly reduce 95th percentile queues, especially for the eastbound approach (850+ feet to 300 feet).

While safety will be enhanced, no significant operational improvements are realized at the Bank Street/Klarides Village signalized driveway. However, the westbound queues will be reduced by 75% during the morning peak hour, and the eastbound queues can be reduced by approximately half.

6.2 <u>Bank Street/Old Drive (west)</u>

Originally, VHB recommended adding a signal at the Bank Street/Old Drive (west) intersection. Upon development of a Walgreens, this intersection was upgraded. While the signal was added, our analysis has determined that the signal timing needs to be adjusted to accommodate the improvements proposed herein.

This signalized intersection has a single westbound lane, one eastbound through lane, and one eastbound left-turn lane along Bank Street. The southbound Old Drive approach has a single approach and departure lane. A sidewalk exists along the southerly side of Bank Street and the easterly side of Old Drive. Pedestrian ramps are present at the eastern leg of the intersection, but no crosswalk has been marked. Pedestrian push buttons and signal heads are located at the northeast and southeast corners. The pedestrian signal phase operates concurrently with the Old Drive green phase.



Modification of the signal timing at this intersection is recommended. A shorter cycle length (60 seconds, down from 90 seconds) will enhance operations from LOS F to LOS C and will significantly reduce queues at all approaches. An increase in the percentage of green time for the Bank Street east/west movements and a reduction of the Old Drive southbound green time will enhance operations.

During the weekday afternoon peak hour, the Bank Street/Old Drive (west) intersection improves from LOS F to LOS C. The eastbound queues can be reduced by approximately 300 feet and the westbound queues by 350 feet. Morning peak-hour operations will remain unchanged; however, the westbound queues will be reduced by approximately 45 feet.

7.0 <u>Mitigation Analysis</u>

The effects of these recommendations on LOS for the peak periods are summarized in Tables 9 through 12.



TABLE 9

2031 Level of Service/

Queuing Impacts of Recommendations Weekday Morning Peak Hour

Signalized Intersections

APPROACH	NO B	UILD	WITH IMPROVEMENTS			
ALI KOACII	LOS	QUEUE ^a	LOS	QUEUE		
Bank St	reet/River Stree	t/Franklin Street				
Eastbound (Bank Street)	A	146	A	120		
Westbound left/through (Bank Street)	С	190	В	154		
Westbound right (Bank Street)	В	53	A	41		
Northbound left (River Street)	С	102	С	110		
Northbound through/right (River Street)	С	40	D	41		
Southbound left (Franklin Street)	С	63	C	69		
Southbound through (Franklin Street)	D	36	D	37		
Southbound right (Franklin Street)	В	39	C	47		
Overall	В		В			
Ва	ank Street/Old D	rive (west)				
Eastbound left (Bank Street)	A	5	A	5		
Eastbound through (Bank Street)	A	185	A	185		
Westbound (Bank Street)	В	173	A	128		
Southbound (Old Drive)	D	100	D	100		
Overall	A		A			
Bank Stre	et/Klarides Villa	ge Main Drivew	ay			
Eastbound (Bank Street)	A	362	A	362		
Westbound left (Bank Street)	A	7	A	2		
Westbound through (Bank Street)	A	76	A	21		
Northbound left (plaza driveway)	D	46	D	46		
Northbound right (plaza driveway)	В	27	В	27		
Overall	A		A			

^a 95th percentile queue in feet

TABLE 10

2031 Level of Service/

Queuing Impacts of Recommendations Weekday Morning Peak Hour

Unsignalized Intersections

APPROACH	NO B	UILD	WITH IMPROVEMENTS					
THE ROME!	LOS	QUEUE ^a	LOS	QUEUE				
В	ank Street/Old L	Prive (east)						
Eastbound left (Bank Street)	A	1	A	1				
Bank Street/Church Street/Beecher Street								
Westbound left (Bank Street)	В	11	В	11				
Northbound (Church Street)	D	55						
Northbound left (Church Street)			D	11				
Northbound right (Church Street)			С	31				
Bank Street/K	Tlarides Village i	unsignalized dri	veway					
Westbound (Bank Street)	A	8	A	8				
Northbound (plaza driveway)	С	25	C	25				

^a 95th percentile queue in feet

TABLE 11

2031 Level of Service/

Queuing Impacts of Recommendations Weekday Afternoon Peak Hour **Signalized Intersections**

APPROACH	NO B	UILD	WITH IMPROVEMENTS			
AFFROACH	LOS	QUEUE ^a	LOS	QUEUE		
Bank Si	reet/River Stree	t/Franklin Street				
Eastbound (Bank Street)	С	326	С	337		
Westbound left/through (Bank Street)	F	465	С	321		
Westbound right (Bank Street)	С	166	В	127		
Northbound left (River Street)	С	259	D	302		
Northbound through/right (River Street)	D	141	D	143		
Southbound left (Franklin Street)	С	135	C	150		
Southbound through (Franklin Street)	С	65	D	70		
Southbound right (Franklin Street)	С	154	C	195		
Overall	Е		С			
Bo	ank Street/Old D	rive (west)				
Eastbound left (Bank Street)	A	18	A	7		
Eastbound through (Bank Street)	В	479	A	184		
Westbound (Bank Street)	F	1083	D	728		
Southbound (Old Drive)	D	111	C 83			
Overall	F		С			
Bank Stre	et/Klarides Villa	age main drivew	ay			
Eastbound (Bank Street)	D	857	В	302		
Westbound left (Bank Street)	A	5	A	3		
Westbound through (Bank Street)	В	182	A	137		
Northbound left (plaza driveway)	D	91	D	87		
Northbound right (plaza driveway)	В	35	В	30		
Overall	С		A			

^a 95th percentile queue in feet

TABLE 12 2031 Level of Service/

Queuing Impacts of Recommendations Weekday <u>Afternoon</u> Peak Hour Unsignalized Intersections

APPROACH	NO B	UILD	WITH IMPROVEMENTS					
ni i koncii	LOS QUEUE ^a		LOS	QUEUE				
В	ank Street/Old L	Prive (east)						
Eastbound left (Bank Street)	С	2	С	2				
Bank Street/Church Street/Beecher Street								
Westbound left (Bank Street)	В	30	В	32				
Northbound (Church Street)	F	205						
Northbound left (Church Street)			F	52				
Northbound right (Church Street)			D	40				
Bank Street/Klarides Village unsignalized driveway								
Westbound (Bank Street)	A	24	A	24				
Northbound (plaza driveway)	С	50	С	57				

^a 95th percentile queue in feet

The intersection of Bank Street/Franklin Street/River Street will experience an overall operational improvement from LOS E to LOS C during the afternoon peak hour. This is primarily due to improving the westbound through traffic. By providing additional time for this movement, the operations will improve from LOS F to LOS C during the afternoon peak hour. The afternoon queues at this approach have also been reduced by approximately 220 feet, and the morning queues also show improvement.

During the weekday afternoon peak hour, the Bank Street/Old Drive (west) intersection improves from LOS F to LOS C. The eastbound queues can be reduced by approximately 300 feet and the westbound queues by 350 feet. Morning peak-hour operations will remain unchanged; however, the westbound queues will be reduced by approximately 45 feet.

While safety will be enhanced, no significant operational improvements are realized at the Bank Street/Klarides Village signalized driveway. However, the westbound queues will be reduced by



75% during the morning peak hour, and the eastbound queues can be reduced by approximately half.

The addition of a lane to the Church Street approach to Bank Street will allow motorists turning right to minimize delays associated with left-turning vehicles. This will reduce morning peak-hour queues by approximately 40 feet and afternoon peak-hour queues by nearly 150 feet. The two-lane configuration will yield afternoon operations of LOS D for right-turning vehicles, which is an improvement from the LOS F condition experienced by the single-lane approach.

8.0 Pedestrian Circulation Summary

An important component of the project was to analyze pedestrian mobility and connectivity along the Route 67 corridor and its connection to downtown Seymour. An evaluation of pedestrian infrastructure was conducted on July 29, 2011 to identify pedestrian-related issues and connectivity gaps. The Seymour/Route 67 Site Analysis Summary is attached in the Appendix. The following is a summary of the findings and recommendations for pedestrian and streetscape enhancements.

In general, the study area does not effectively provide for safe pedestrian mobility throughout. While a sidewalk network exists, many areas are in disrepair, crosswalks are not handicap compliant, and gaps exist in many areas making it unsafe for pedestrians to travel from Klarides Village and points west to downtown Seymour. Sidewalk and crosswalk improvements have been made over the past few years but are site specific to development sites such as the new Walgreens. The primary challenge of connecting the Bank Street corridor to downtown Seymour is the Route 8 interchange that separates these two areas. Safety measures, physical improvements, and streetscape enhancements are needed in order to encourage pedestrian activity. There are many unique features including three parklet areas within the study area, which provide opportunities to create linkages and a safer and much more inviting experience for pedestrians. Additionally, the Tingue Dam fish bypass channel and park in downtown Seymour (currently under construction), which will be accessed via Deforest Street, offers an additional



pedestrian destination. This project will permit river access at the mouth of a new fish bypass channel in conjunction with park improvements and provide a unique recreational and educational experience along the Naugatuck River.





Tingue Dam Fish Bypass and Park Currently Under Construction

Tingue Dam Overlook

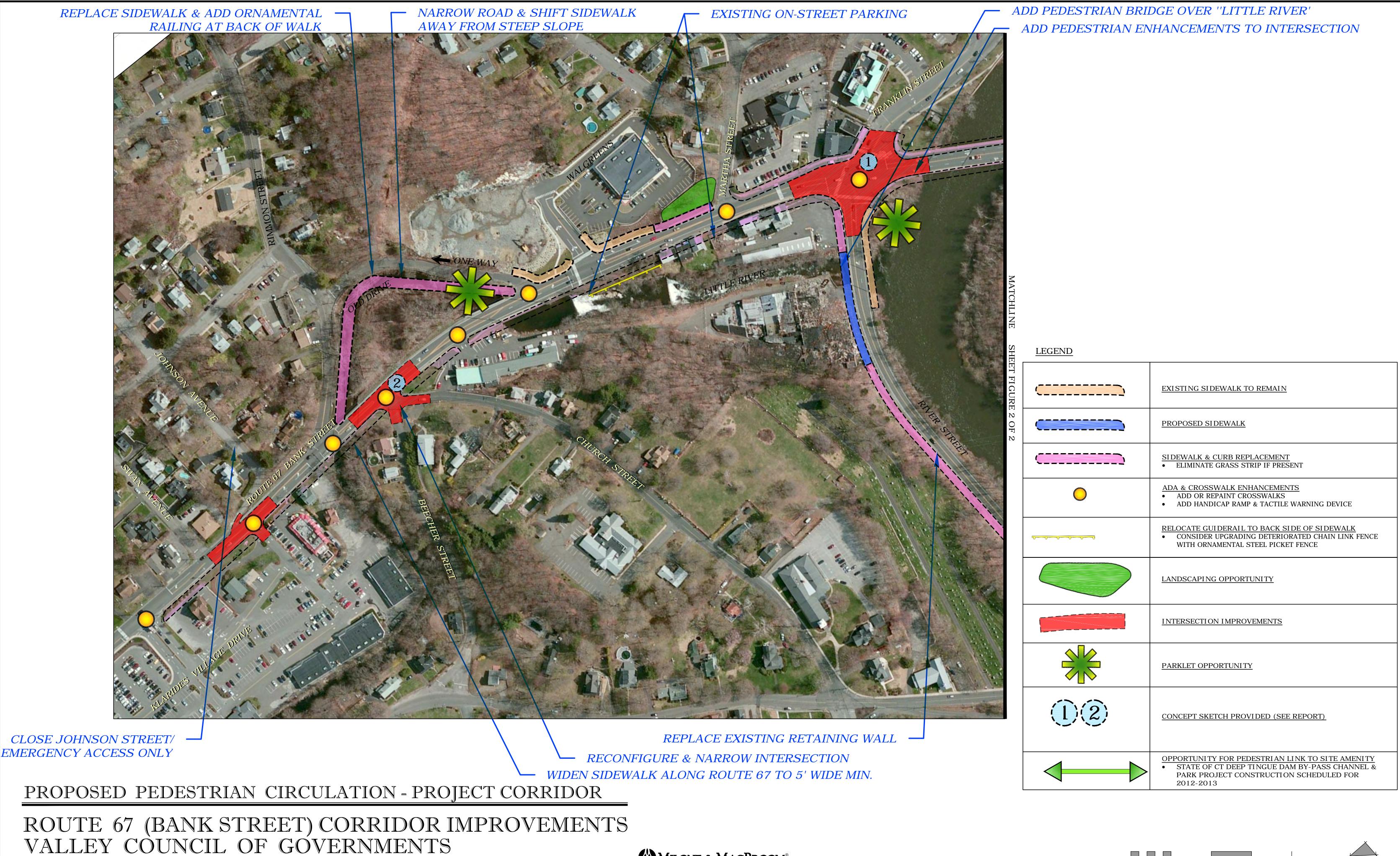
Figures 12 and 13 graphically depict the pedestrian circulation gaps and proposed improvements for Bank Street to downtown Seymour. The following summarizes the common issues and opportunities found within the study area.

Americans With Disabilities Act (ADA) Compliance Issues – The majority of crosswalks need enhancements such as simply repainting the crosswalk or adding handicap ramps and/or tactile warning devices in order to comply with current ADA standards. Crosswalks are needed at each major commercial driveway curb cut or intersecting roadway. The intersection at Old Drive West and

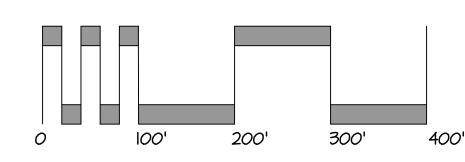


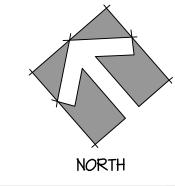
Bank Street needs a painted crosswalk across Bank Street. Due to steep slopes and right-of-way constraints, sidewalks are not feasible along the northerly side of Bank Street. Therefore, pedestrians are required to cross at this intersection. While a tactile warning device is present, there is no marked crosswalk.

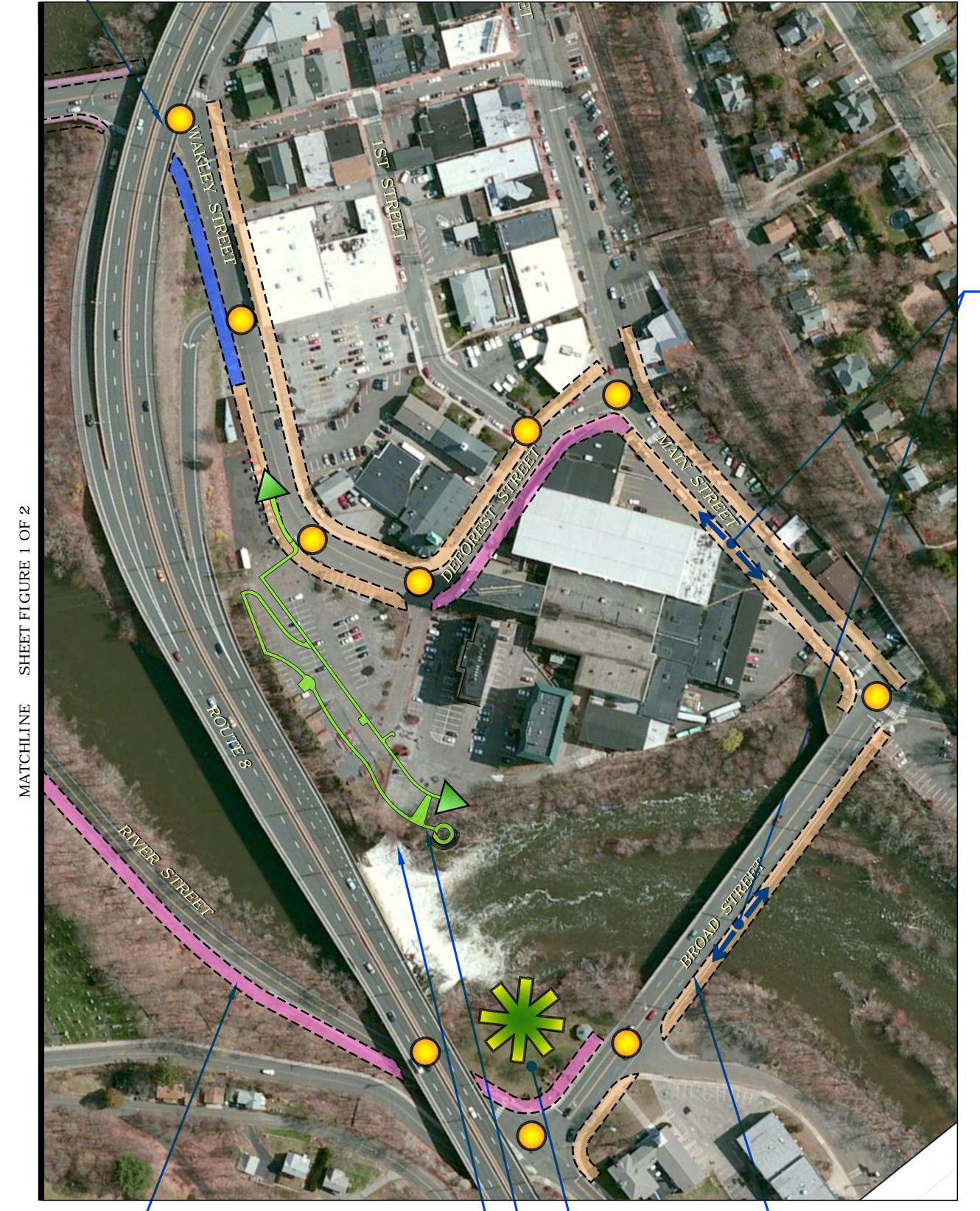




MILONE & MACBROOM®







EXISTING SIDEWALK TO REMAIN

LEGEND

LEGEND	
	EXISTING SIDEWALK TO REMAIN
	PROPOSED SI DEWALK
	SIDEWALK & CURB REPLACEMENT • ELIMINATE GRASS STRIP IF PRESENT
	ADA & CROSSWALK ENHANCEMENTS ADD OR REPAINT CROSSWALKS ADD HANDICAP RAMP & TACTILE WARNING DEVICE
	RELOCATE GUI DERAIL TO BACK SIDE OF SIDEWALK OCONSIDER UPGRADING DETERIORATED CHAIN LINK FENCE WITH ORNAMENTAL STEEL PICKET FENCE
	LANDSCAPING OPPORTUNITY
	INTERSECTION IMPROVEMENTS
	PARKLET OPPORTUNITY
(1)(2)	CONCEPT SKETCH PROVIDED (SEE REPORT)
	OPPORTUNITY FOR PEDESTRIAN LINK TO SITE AMENITY • STATE OF CT DEEP TINGUE DAM BY-PASS CHANNEL & PARK PROJECT CONSTRUCTION SCHEDULED FOR 2012-2013

REPLACE EXISTING SIDEWALK W/10' WIDE MULTI - USE TRAIL & ADD PROPOSED IMPROVEMENTS, LIGHTS, BENCHES, ETC.

PROPOSED PEDESTRIAN CIRCULATION - DOWNTOWN

ROUTE 67 (BANK STREET) CORRIDOR IMPROVEMENTS VALLEY COUNCIL OF GOVERNMENTS

DOWNTOWN AREA & ROUTE 67 WEST TO KLARIDES VILLAGE SEYMOUR, CONNECTICUT FEBRUARY 2014

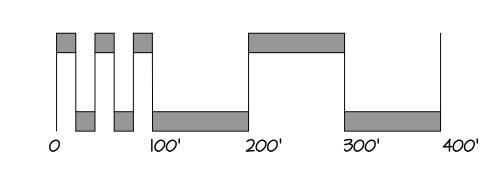
- PAINT BRIDGE RAILING BLACK & ADD PEDESTRIAN LIGHTING

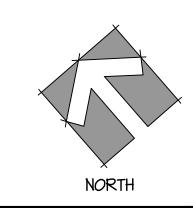
- 2012 BROAD STREET PARK RENOVATIONS

TINGUE DAM PROJECT (SEE LEGEND)

CREATE PEDESTRIAN CONNECTION TO TINGUE DAM







Sidewalk and Streetscape Enhancements – Sidewalk and streetscape enhancements should be considered along the Bank Street corridor and downtown Seymour for pedestrian safety and for creating an aesthetically pleasing experience for all modes of travel. It should also be noted that the introduction of certain streetscape improvements has been proven to affect traffic calming.



A sidewalk network exists along Bank Street; however, there are areas where the concrete is broken, mulch and landscaping debris are present on the walkway, and vegetation overburden impacts useable sidewalk widths. Therefore, these sidewalks should be addressed. The decision to replace curbing should be evaluated on a case-by-case basis.

The downtown sidewalk network is generally in better condition than that of Bank Street. However, the sidewalks that provide the connection to downtown by way of Bank Street and River Street are also in disrepair and will require improvements. Currently, these sidewalks are unsafe and in some instances are poorly illuminated, adversely affecting safe pedestrian mobility.

The following treatments/improvements are recommended:

- Replace all concrete walks along Bank Street and "as needed" in the downtown area
 with the exception of the new walk along the frontage of Walgreens.
- Replace curbing (granite, cost permitting, and on a case-by-case basis).
- Add decorative pedestrian-level lighting where feasible and appropriate.
 (Illumination below the Route 8 overpass may be deemed critical.)
- Add trees and shrubs where feasible and appropriate.
- Extend landscape treatments along the slope on Bank Street between Walgreens and Martha Street - see images below.







Streetscape enhancements should be consistent throughout the study area. This will create a sense of place and character that the Bank Street corridor currently does not have, encourage more pedestrian use, and assist in traffic calming.

8.1 <u>Unique Opportunities</u>

A prominent downtown feature and natural resource to the town of Seymour is the Naugatuck River. The Naugatuck River and its tributaries provide recreational opportunities and destinations throughout the study area. There are two locations along Bank Street and one location in downtown Seymour that utilize the Naugatuck River and its tributary as scenic recreational refuges.

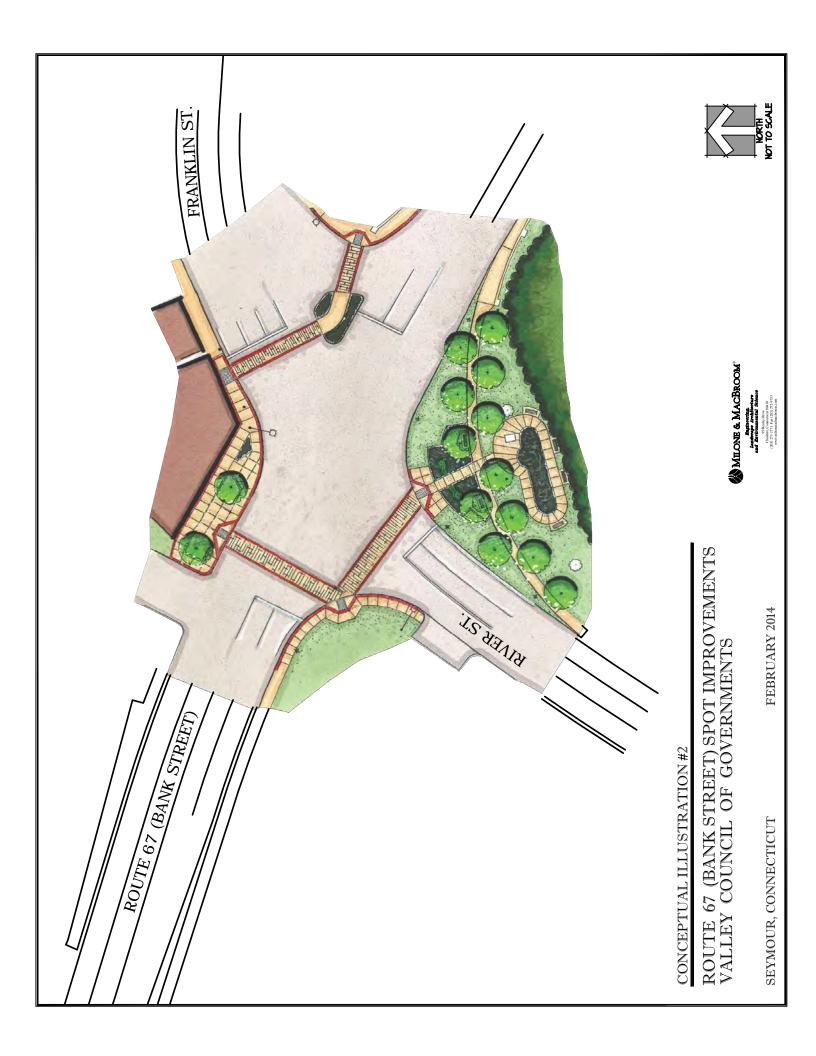
The first is located at the intersection of River Street, Franklin Street, and Bank Street. A small parklet exists at the southeast corner of the intersection that overlooks the river. Along with roadway improvements, this area can be enhanced by adding more recreational space and updating the park area to become more inviting (see Conceptual Illustration #2).

A second parklet opportunity is located along Old Drive East. This parklet is accessed by the sidewalk/trail that loops around the river bend and connects back to Bank Street along Old Drive West.

There are serious safety concerns along this loop. The timber railings are unstable and do not meet current code requirements,







and the trail itself is set so close to the drop-off of the embankment that it creates a potential serious liability. Since Old Drive East is now a one-way street, the roadway may be narrowed, moving this path away from the steep drop-off and replacing the railings.

The third parklet is located in the downtown area at the corner of River Street and Broad Street. This parklet overlooks the Tingue Dam from the west. In 2012, renovations of the Broad Street park were initiated providing a 500-foot brick walkway, benches overlooking the dam and Naugatuck River waterfalls, and lighting for safety. With these improvements, this parklet further enhances the downtown Seymour experience and enjoyment of the river.

Lastly, the Tingue Dam fish bypass and associated park feature currently being constructed will create a recreational park area in downtown Seymour that overlooks the dam. This is expected to bring visitors and create a sense of place in the downtown.

9.0 Other Corridor Improvement Projects

In addition to the projects mentioned above that are being pursued within or adjacent to the limits of this study, recently, the CTDOT advertised and received bids for the Rehabilitation of Bridge No. 01061 Route 67 Over Little River (CTDOT Project No. 124-167). This structure crossing is immediately west of Old Drive East and the Walgreens signalized intersection. As indicated in the inspection reports for this structure, the bridge has been given a poor rating given the condition of the existing superstructure. The proposed rehabilitation will include:

- Replacement of the expansion joints at both abutments
- Replacement of the concrete-filled steel grid sidewalk and cantilevered sidewalk stringers
- Painting of the exposed structural steel and steel members along the walkway
- Repairs to the deteriorated concrete surfaces on the superstructure and substructure

The replacement of the cantilevered walk and pedestrian railing will slightly narrow the width of the walkway from 7'-0" clear to 6'- $5^{3/8}$ ". The existing water main, which is hung underneath the



sidewalk, will also be replaced as part of that project. While the sidewalk replacement maintains the current pedestrian access across the bridge, given the width of the bridge and the location of the through-girder/steel parapet in relation to the minimum Route 67 lane geometry, the bridge superstructure, unless replaced and widened, currently cannot support a widened shoulder or wider sidewalk, which would allow for a shared-use path or on-street bicycle continuity. Also, the existing lane configuration and limited shoulder widths west of this bridge also limit on-road bicycle continuity. Based upon a cursory review of the structure drawings, it appears that a similar cantilevered sidewalk could be constructed on the north/upstream side of the bridge. While on-street bicycle opportunities to the west are limited, as discussed earlier in this report, there are opportunities to establish bicycle connections between the residential areas served by Old Drive/Rimmon Road and the Bank Street and larger downtown Seymour area.

10.0 Summary

As outlined within this report, some of the original recommendations by VHB have been implemented, and our recent analysis will help advance the implementation of the remaining recommendations. Several design alternatives have been presented within this report, some more challenging than others. Attached in the Appendix of this report are preliminary cost opinions for each of the preferred alternatives, summarized individually and collectively for funding purposes. The amounts have been adjusted for inflation assuming a construction year of 2019.

Similar to most municipal downtown centers, the options outlined to improve traffic and safety along the corridor must also consider the impacts to and the needs of the adjacent residences and businesses, future redevelopment, and other interested or affected stakeholders. Also, while streetscape enhancements may have to be phased, attempts should be made to incorporate these improvements into each stand-alone project as it is advanced.

This report has highlighted the issues and opportunities to not only improve the traffic operations but also the pedestrian circulation network that connects Route 67 (Bank Street) to the adjacent neighborhoods, Seymour's downtown area, and nearby riverfront resources. Using the



information provided herein, the VCOG and Town of Seymour will be able to develop priorities within the corridor, identify available funding sources to implement the improvements, and integrate these improvements with current and future redevelopment initiatives.

3211-02-4-mr1516-rpt





Valley Council of Governments
Preliminary Opinion of Costs - Preferred Alternates
Route 67 (Bank Street) Spot Improvements
Seymour, CT

State Project No. 124-165 February 2014

Improvement Location		Cost							
(see attached for specific breakdown)									
	_		-						
Johnson Street Access Termination	\$	52,280.00	-						
Klarides Plaza Entrance	\$	26,785.00	1						
			4						
Church St. / Beecher St. Realignment	\$	149,400.00	-						
Route 67 - Old Drive to River St. Int.	\$	734,330.00	1						
Southeast corner of Bank/River St. Int.	\$	148,235.00							
River St. (SR 313) Widening - inc. bridge	\$	726,250.00							
subtotal	\$	1,837,280.00	4						
Traffic Items 3%	\$	55,118.40	1						
Minor Items 25%	\$	459,320.00	-1						
subtotal	\$	2,351,718.40							
Clearing & Grubbing, M&PT, Trafficperson, & Construction Staking included in each lo									
Inflation (4%/year) 2019 Construction	\$	509,506.62	-1						
subtotal	\$	2,861,225.02	1						
Contingencies (<\$5,000,000 : 10%)	\$	286,122.50	1						
Incidentals (\$1-5million : 25%)	\$	715,306.25	-1						
Utilities (Estimated)	\$	100,000.00							
Total Construction Cost	\$	3,962,653.77							
				1 /0/	١٥/١	04.	1 - /400/)	T	14.0
		Total Cost	Fе	deral (80	J%)	518	ate (10%)	10	vn (10





Pedestrian Opportunities and Constraints Bank Street to Downtown Seymour

Pedestrian accessibility is an important component of the RT 67 corridor study in Seymour, CT. On July 29, 2011 the entire study area was walked and pedestrian related issues were documented using digital photography and field notes. To facilitate understanding theses issues and where they occur we will start from the western limit of work, at the Klarides Village Shops and proceed easterly down Bank Street, then cross the bridge and pass beneath Route 8, turning south down Wakely Street, then turning east along Deforest Street, then turning south along Main Street, then turning west along Broad Street (passing over the bridge), then passing beneath Route 8 and proceeding north along River Street, returning to the intersection of River Street and Bank Street. We performed further visual analysis along Franklin Street, traveling north to approximately the Stop 'n Shop store. In this area we focused on the existing sidewalks and park-like area to the east of Franklin Street (adjacent to the Naugatuck River).

An existing walk system along Old Drive (adjacent to Little River) provides for pedestrian movement along the north side of Bank Street where no sidewalks currently exist. We will report our findings along this section of road at the end of this study.

In addition to supporting graphics prepared as part of this phase of the project, this report will provide additional photographs to depict unique or special conditions.



S. Side of Bank Street at Klarides

- Bituminous concrete sidewalks in poor condition and approx. 5' wide
- Curb reveal is less than 6"
- Mulch from adjacent landscape bed is migrating onto walk – need for curb at
- Abandoned curb cut



S. Side of Bank Street at Klarides Entrance

- Crosswalk does not meet current standards
- Drop curbs missing ADA tactile warning strips



N. Side of Bank Street at Klarides

- No ADA tactile warning strip at crosswalk
- Ped signal, but no sidewalk along north side



S. Side of Bank Street south of Klarides

- · Concrete walk in good condition
- Grass strip at edge of road is maintenance problem
- Consider extending walk to back of curb
- Adequate space for site lighting (minimal overhead conflicts)



Pedestrian Crossing at Bank and Old Drive

- No dedicated painted crosswalk
- No ADA tactile warning strip on south side of Bank Street
- Note: no sidewalk exists along the north side of Bank Street
- This crossing provides ped. Access to the walk along Old Drive



S. Side of Bank Street at Allen's Plumbing Supply

- No painted crosswalk
- Drop curbs missing ADA tactile warning strips



S. Side of Bank Street Adjacent to Little River

- On-street parking is an advantage
- Existing guiderail conflicts with ease of pedestrian movement from the car to the sidewalk (as well as the swing of the car door)
- Narrow bituminous sidewalk in poor condition
- Chain link fence is uninviting consider optional fence treatment



N. Side of Bank Street at Klarides

- No ADA tactile warning strip at crosswalk
- Ped signal, but no sidewalk along north side



N. Side of Bank Street at Walgreens

- Concrete walk in good condition
- Bank plantings have stabilized slope



N. Side of Bank Street East of Walgreens

- Slope treatment low visual appeal and doesn't match treatment at Walgreens.
- · Concrete sidewalk in fair condition



S. Side of Bank Street at Ed's Cleaners

- Curb reveal is less than 6" high
- Bituminous concrete sidewalk in poor condition
- Consider expanding new surface treatments to the building façade
- · Opportunity for new bench and trash receptacle



N.Side of Bank St. at Martha St. Intersection

- Concrete and curb in poor condition
- Bituminous concrete road and gutter have failed
- No painted crosswalk or accessible ramps with tactile warning strip



S.Side of Bank Street at Seymour Lumber Co.

- Opportunity to work with developer to enhance streetscape treatments
- Good opportunity to establish streetscape theme here and at the intersection



N. Side of Bank Street Approaching RT 313 Intersection

- Concrete sidewalk and curb in poor condition with minimal curb reveal
- Wall in need of repair
- Unsafe mid-block crossing is visible
- No ADA compliant drop curbs/ramps or tactile warning strips



Pedestrian Crossing at Intersection of Bank and Franklin

- Crosswalks are poorly defined
- No ADA drop curb/ramp or tactile warning strips
- Note: no sidewalk exists along the north side of Bank Street
- This crossing provides ped. Access to the walk along Old Drive



Pedestrian Crossing at Intersection of Bank and Franklin

- Excessively wide street crossing with no area of pedestrian refuge
- Consider bump out at end of on-street parking to shorten distance



Pedestrian Areas and Crosswalks Below Rt 8

- Area is a sea of pavement and is poorly lighted
- · Poorly defined pedestrian movements
- Opportunity to introduce new paving treatments and lighting
- Majority of pedestrian crosswalks are lacking ADA compliant tactile warning strips



West Side of Wakely Street

 Opportunity for construction of new sidewalks and streetscape enhancements



W. Side of Wakely Street at Office Building

- Opportunity to continue dedicated pedestrian walk through parking lot
- Adequate room exists to adjust the limits of paved parking lot to enhance safe pedestrian movement



W. Side of Wakely Street at Parking Lot Adjacent to RT 8 and Future Tingue Dam Improvements

- Existing concrete walks and bituminous curb in poor condition
- Establish safe dedicated pedestrian access to waterfront improvements at Tingue Dam



Intersection of Wakely and DeForest Streets

- No painted crosswalk
- No accessible Drop curbs/ramps and missing ADA tactile warning strips
- Existing brick walking surface is uneven, but visually inviting compared to other walks in the area.



S. Side of DeForest Street

- Limit of brick paver sidewalk
- Concrete in poor condition
- Curb cut appears to be excessively wide and curb reveal is minimal



Intersection of DeForest and First Streets.

 No dedicated pedestrian crosswalks, or ADA compliant drop curb/ramp with tactile warning strips.



Intersection of DeForest and Main Street

- Lacking dedicated pedestrian crosswalks with accessible drop curb/ramp and tactile warning strips.
- Curb in front of Post Office is excessively high and creates an unsafe condition. Car doors cannot be opened on the sidewalk side of the on-street parking



Main Street Sidewalks Looking South

- Concrete walks and curb on west side of street are generally in good to fair condition
- Concrete walks and curb on east side of street are in poor condition
- Opportunity for introduction of pedestrian-level lighting



Broad Street Bridge Over Naugatuck River

- Metal Bridge Railing is rusted and would benefit from a new coat of paint
- Consideration should be given to providing pedestrian level lighting, which could be attached to the outside of the concrete rail/wall
- Vehicular speeds are high in this location, with minimal safe walking distance from travelway



Curb Cut Along South Side of Broad Street

• No dedicated ADA compliant pedestrian crossing



South Side of Broad Street at Route 8 Underpass

 No ADA compliant pedestrian crosswalk here, which denies safe access to the parklet on the north side of the street



River Street at Bottom of Route 8 Ramp

 No ADA compliant pedestrian crosswalk across River Street or at bottom of ramp.



West side of River Street Looking North

- Existing concrete walks and bituminous curb in poor condition
- Wide grass shelf could accommodate wider sidewalks and other amenities, including new landscape treatments
- · No sidewalks along east side of road



West side of River Street Looking North

- Existing concrete walks and curb in poor condition and very narrow (curb is approx. 2' away from travelway)
- Retaining wall is in very poor condition. Wall ranges in height from approx. 1' to 5'
- Possible horizontal realignment of the road in the direction of the river would permit widening of the walk.



West Side of River Street at Lumber Co.

 Presently no sidewalk exists. It is presumed that this will be corrected as part of the site plan approval process for the new development



Little River Bridge at West Side of River St.

- No sidewalk at this location
- Consider new prefabricated pedestrian bridge to be located adjacent to the existing concrete bridge
- Existing bridge structure should be evaluated for structural integrity



Franklin Street Looking North to Stop n Shop

- Sidewalk along west side of Franklin terminates with no pedestrian linkage to Stop n Shop
- · Existing concrete sidewalk in poor condition



Parklet Along East Side of Franklin

- Existing sidewalk provides a circuitous route to the Stop n Shop
- Area could benefit from pedestrian-level site lighting.



East side of Old Drive Adjacent to Little River

- Existing bituminous sidewalk is narrow and in fair to poor condition
- Timber fence system is not code compliant (based on vertical drop to water, no openings can be greater than 4").
- Existing mature deciduous trees are generally in good condition and provide for an enjoyable, shady walking experience



East side of Old Drive Adjacent to Little River

- A single pedestrian opening at the intersection does not provide for safe discharge at the intersection.
- No crosswalks



East side of Old Drive Adjacent to Little River

- Vertical drop to river is treacherous
- Structural integrity of the existing cobble wall should be performed



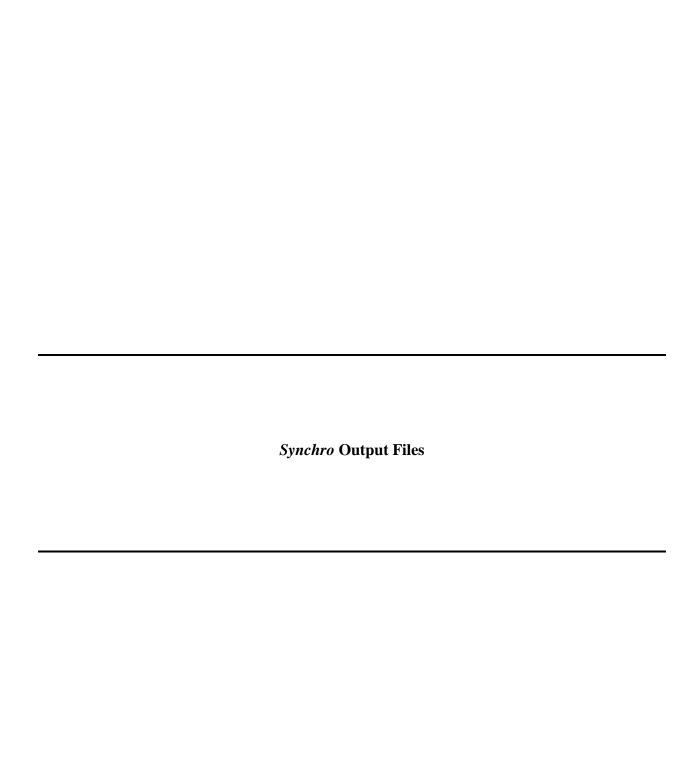
Old Drive Adjacent to Little River Looking East

- One-way vehicular travel
- Road width appears adequately wide to provide for wider, enhanced sidewalks along the water side.



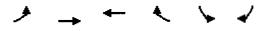
East side of Old Drive Adjacent to Little River

 Small level lawn area at the end of Old Drive provides an opportunity for a small parklet.





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Turn Bay Length (ft)	100			
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Oldiago Dap Hodadai		0	0	0
Reduced v/c Ratio	0.04	0.56	0.55	0.38

Area Type:

Other

Cycle Length: 80

Actuated Cycle Length: 80

Offset: 1 (1%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.55

Intersection Signal Delay: 9.8

Intersection LOS: A

ICU Level of Service A

Intersection Capacity Utilization 53.4% Analysis Period (min) 15

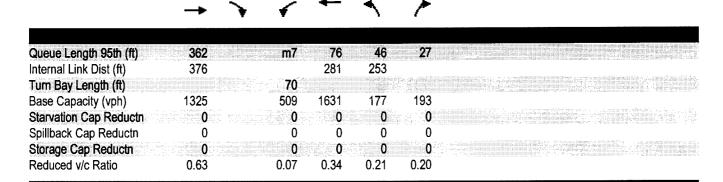
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Splits and Phases: 2: Bank St & Old Dr (west)



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Area Type: Other

Cycle Length: 80

Actuated Cycle Length: 80

Offset: 7 (9%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.63

Intersection Signal Delay: 7.8 Intersection LOS: A Intersection Capacity Utilization 54.5% ICU Level of Service A

Analysis Period (mirr) 15

m Volume for 95th percentile queue is metered by upstream signal.

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Minimum Initial (s)	6.0			15.0	15.0	15.0	6.0	6.0		6.0	6.0	
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Maximum Green (s)	13.0			21.7	21.7	21.7	13.0	13.9		13.0	13.9	
Yellow Time (s)	3.0			3.0	3.0	3.0	3.0	3.9		3.0	3.9	
All-Red Time (s)	1.0			2.5	2.5	2.5	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	4.0	4.0	4.0	5.5	5.5	5.5	4.0	4.9	4.0	4.0	4.9	4.9
Lead/Lag	Lead			Lag	Lag	Lag	Lead	Lag		Lead	Lag	
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Vehicle Extension (s)	0.2			0.2	0.2	0.2	2.0	2.0		2.0	2.0	
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Actuated g/C Ratio		0.60			0.27	0.27	0.19	0.10		0.21	0.08	0.42
v/c Ratio		0.54			0.67	0.17	0.50	0.19		0.26	0.18	0.08
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Internal Link Dist (ft) 129		742			541			472	
Turn Bay Length (ft)			25	230			300		300
Base Capacity (vph) 1845		857	512	353	318		394	313	682
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Spillback Cap Reductn 0		0	. 0	0	0		0	0	0
Storage Cap Reductn 0		0	0	0	0		0	0	0
Reduced v/c Ratio 0.54		0.67	0.17	0:43	0.10		0.22	0.09	0.08

Other

Cycle Length: 80

Actuated Cycle Length: 80

Offset: 46 (58%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 55

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.67

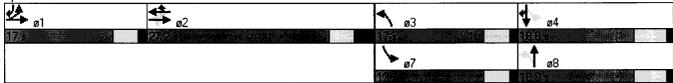
Intersection Signal Delay: 18.2

Intersection Capacity Utilization 67.0%

Intersection LOS: B
ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 11: Bank St & Franklin St



	→	•	•	•	•	~				
÷		-	-		_	-				
Lane Configurations	ĵ.			ર્ન	¥f					
Volume (veh/h)	690	30	70	555	- 5	90				
Sign Control	Free			Free	Stop					
Grade	0%			0%	0%					
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92				
Hourly flow rate (vph)	750	33	76	603	5	98				
Pedestrians	and the new training and a				at in a casa na cananana		onamanian padalahiyi iyi			
Lane Width (ft)										
Walking Speed (ft/s)			on overse var oader							
Percent Blockage										
Right turn flare (veh) Median type	None			None						
Median storage veh)	INUITE			INDITE						
Upstream signal (ft)	361	re og til pyrmed Rud Arthur		275						
pX, platoon unblocked	XX 1		0.73		0.84	0.73			y,0000000000000000000000000000000000	
vC, conflicting volume			783		1522	766				
vC1, stage 1 conf vol										
vC2, stage 2 conf vol										
vCu, unblocked vol			518		946	496				
tC, single (s)			4,1		6.4	6.2				
tC, 2 stage (s)				es sacionalism (inc			·			grotege ledtige wilde
tF (s)			2.2		3.5	3,3				
p0 queue free %		u rozali estor	90 766	."	98 219	77 419			n Samuella and S. (177)	
cM capacity (veh/h)		alde Jeens	/00		248					
parties and										
Volume Total	783	679	103							
Volume Left	0	76	5			anto di Saladi de Pali de Nacional de Compa				
Volume Right cSH	33 1700	0 766	98 400							
Volume to Capacity	0.46	0.10	0.26							
Queue Length 95th (ft)	0.40	8	25							
Control Delay (s)	0.0	2.5	17.1			inaca kappahilin				
Lane LOS	programmer	Α	C				HERSOTERALISMA 1 15			
Approach Delay (s)	0.0	2.5	17.1							
Approach LOS			С	er teather to the entire						
48 \$ 17 6 A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1										
Average Delay			2.2							
Intersection Capacity Utilizat	ion		87.1%	ic.	U Level d	of Service		- ARE		
Analysis Period (min)			15				manazez z iili (Funci			Jacobson Central Central Alberta

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			•		-	•	
ane Configurations	ĵ >		ሻ	†	¥		
/olume (veh/h)	825	30	80	595	20	90	
Sign Control	Free			Free	Stop		
Grade	0%			0%	- 0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	897	33	87	647	22	98	
Pedestrians			Harisaa st	1-4799399999			
ane Width (ft)							
Walking Speed (ft/s) Percent Blockage							
Right turn flare (veh)							
Median type	None			None			
Median storage veh)							
Jpstream signal (ft)	175			1318			
X, platoon unblocked			0.80		0.90	0.80	
C, conflicting volume			929		1734	913	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol						and the state of t	
vCu, unblocked vol			785		1253	765	
C, single (s)			4.1		6.4	6.2	
C, 2 stage (s)			2.2		3.5	3.3	
tF (s) p0 queue free %			2.2 87		85	70	
cM capacity (veh/h)			665		148	322	
	era e compine di	et. Costillani					
Volume Total	929	87	647	120			
Volume Left	0	87	0	22			
/olume Right	33	0	Ŏ	98			
:SH	1700	665	1700	265		S of Computational Computation of the Computation o	
Volume to Capacity	0.55	0.13	0.38	0.45			
Queue Length 95th (ft)	0	11	0	55			
Control Delay (s)	0.0	11.2	0.0	29.3	arty Dale		
ane LOS	s addana i	В		D	ES LA ELFRAPATRE A LA	EASTERSULE volve aviso, is a many manufall manufalistic statement of a second communication of the second statement of the sec	
Approach Delay (s) Approach LOS	0.0	1.3		29.3 D			
• •							
Average Delay			2.5				
Average Delay Intersection Capacity Utiliza	ation		66.3%	חו	ا امیم ا	of Service C	
Analysis Period (min)	auOII		15		O FRAGIC		
analysis relied (IIIII)			ΙÜ		**************************************		

	٦	→	+	4	\	4
•						
Lane Configurations	ሻ	†	1>			
Volume (veh/h)	5	915	670	25	0	O market in the second of the
Sign Control		Free	Free		Stop	
Grade	0.00	0%	0%	0.00	0%	0.02
Peak Hour Factor	0.92 5	0.92 995	0.92 728	0.92 27	0.92 0	0.92 0
Hourly flow rate (vph) Pedestrians	J.	990	120	21	U	
Lane Width (ft)						
Walking Speed (ft/s)						
Percent Blockage						
Right turn flare (veh)						
Median type		None	None			
Median storage veh)	··					
Upstream signal (ft)		612	881			
pX, platoon unblocked	0.76	erages com-rh			0.87	0.76
vC, conflicting volume	755				1747	742
vC1, stage 1 conf vol	-51233460000					
vC2, stage 2 conf vol vCu, unblocked vol	525				1213	507
tC, single (s)	4.1				6.4	6.2
tC, 2 stage (s)			. 11 Feb. 5800000		Y.	
tF (s)	2.2				3.5	3.3
p0 queue free %	99				100	100
cM capacity (veh/h)	795				174	432
antychnican						
Volume Total	5	995	755			
Volume Left	5	0	0			
Volume Right	0	0	27			
cSH	795	1700	1700			
Volume to Capacity	0.01	0.59	0.44			
Queue Length 95th (ft)	1	0	0			- 1, 11, 21, 1469 op 21 mboer van en noorgamen modere hellinkelijk 9454605 kaan van de 'n oarste men en meerste oordel 1,
Control Delay (s)	9.6	0.0	0.0			
Lane LOS	A					
Approach Delay (s) Approach LOS	0.1		0.0			
Application LOS						
Average Delay			0.0			Tarah menganya mangga 1 sa sa Jamah mengangan mengangan mengangan menggan menggan menggan sa sa sa sa sa sa sa
Intersection Capacity Utiliza	ition		51.5%	ıC	U Level o	of Service A
Analysis Period (min)			15	e e re namenammana na	talk to all her to be a fee	

1 100000	۶	→	+	4	\	4
Lane Configurations	ሻ	∱	1 >		¥¥	
Volume (vph)	40	880	1140	5	70	35
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (ft)	100			0	0	0
Storage Lanes	1		fallet after a dit stere	0	1	0
Taper Length (ft)	25			25	25	25
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fitalis de la	1.00	1.00	0.999		0.955	
Fit Protected	0.950		0.000		0.968	Biller (1997) - 1990 - Albertania Balling (1997) - 1990 - 1990 - Albertania Balling (1997) - 1990 - 1990 - 199 Biller (1997) - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990 - 199
Satd. Flow (prot)	1770	1863	1861	0		0
Fit Permitted	0.086	1000	1001	U	0.968	
		4000	4004	A		
Satd. Flow (perm)	160	1863	1861	0	1722	0
Right Turn on Red				No		No
Satd. Flow (RTOR)						
Link Speed (mph)	er er lærlærege	30	30		30	
Link Distance (ft)		275	175		403	
Travel Time (s)		6.3	4.0		9.2	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	43	957	1239	5	76	38
Shared Lane Traffic (%)						
Lane Group Flow (vph)	43	957	1244	0	114	0
Turn Type	pm+pt					
Protected Phases	1	12	2		4	
Permitted Phases	12	2				
Detector Phase	1	12	2		4	
Switch Phase						
Minimum Initial (s)	3.0		15.0		7.0	nningsal (1919). Est bereinningsbring neumanning minningsbringsbringsbring bis bis 1996 sein de market in de m The state of the state o
Minimum Split (s)	6.1		20.0		11.0	
Total Split (s)	24.1	61.0	36.9	0.0	29.0	0.0
Total Split (%)	26.8%	67.8%	41.0%	0.0%	32.2%	0.0%
Maximum Green (s)	21.0	01.070	31.9	V.V.0	25.0	
Yellow Time (s)	3.0		3.0		3.0	
All-Red Time (s)	0.1		2.0		1.0	
Lost Time Adjust (s)	0.0	0.0	0.0	nn	0.0	0.0
Total Lost Time (s)	3.1	3.1	5.0	0.0 4.0	4.0	4.0
		ا , ق ا	1.0	4.0	4.0	4.0 Resentante se en el escentir acomo sobri tendro del
Lead/Lag	Lead		Lag			
Lead-Lag Optimize?	4 5	De deligioù de com	ЕА		4 2	
Vehicle Extension (s)	1.5		5.0		1.5	
Recall Mode	None		C-Min		None	
Act Effet Green (s)	71.8	75.5	47.3		10.2	
Actuated g/C Ratio	0.80	0.84	0.53		0.11	
v/c Ratio	0.08	0.61	1.27		0.58	
Control Delay	6.5	12.7	147.3		49.3	The state of the s
Queue Delay	0.0	0.4	0.0		0.0	
Total Delay	6.5	13.1	147.3		49.3	
LOS	A	В	F		D.	
Approach Delay		12.8	147.3		49.3	and a second common control of the second common plantage and distributed to the control of the second control
Approach LOS		В	i F		D	



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Queue Length 95th (ft)	m18	m479 m	#1083	111
Internal Link Dist (ft)		195	95	323
Turn Bay Length (ft)	100			
Base Capacity (vph)	593	1562	979	478
Starvation Cap Reductn	0	190	0	0
Spillback Cap Reductn	0	0	0	0
Storage Cap Reductn	0	0	0	0
Reduced v/c Ratio	0.07	0.70	1.27	0.24

Other

Cycle Length: 90

Actuated Cycle Length: 90

Offset: 1 (1%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 90

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.27

Intersection Signal Delay: 85.5
Intersection Capacity Utilization 73.8%

Intersection LOS: F

ICU Level of Service D

Analysis Period (min) 15

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

- # 95th percentile volume exceeds capacity, queue may be longer.

 Queue shown is maximum after two cycles.
- m Volume for 95th percentile queue is metered by upstream signal.

Splits and Phases: 2: Bank St & Old Dr (west)

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(2) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	TO 070460 ANALOS	72

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	-	•	•		1	.	
Long Configurations	•		*	_	*	7	
Lane Configurations	}	60	ሻ	†	ሻ 80	r 55	
Volume (vph)	705	60 1900	40	940		1900	Programme
Ideal Flow (vphpl)	1900		1900	1900	1900		
Storage Length (ft)		0	70		0	0	
Storage Lanes		0	1 		1 	1	
Taper Length (ft)	400	25	25		25	25	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	
<u>Fn</u>	0.989	Perifekti ing Peripak	0.050		^ ^ - ^	0.850	
Flt Protected			0.950		0.950	· · · · · · · · · · · · · · · · · · ·	
Satd. Flow (prot)	1842	0	1770	1863	1770	1583	
Flt Permitted	the protein graduation is	anagna 😩 -	0.092		0.950		######################################
Satd. Flow (perm)	1842	. 0	171	1863	1770	1583	
Right Turn on Red	Jäggagitakäankintäi ⊑ki. ' '	Yes	.e.ng.ete.t	o un apropopation of		Yes	
Satd: Flow (RTOR)	5	Mik .	uist. ii.			60	
Link Speed (mph)	30			30	30		
Link Distance (ft)	456	rama sür.		361	333		
Travel Time (s)	10.4			8.2	7.6		a ser - 2 Meeti anamaning manamaning manamaning a series series
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	Estimate the control of the control
Adj. Flow (vph)	766	65	43	1022	87	60	
Shared Lane Traffic (%)							
ane Group Flow (vph)	831	0	43	1022	87	60	
Turn Type			pm+pt			Prot	
Protected Phases	2		1	1 2	4	4	
Permitted Phases			12	2	4		
Detector Phase	2		1	1 2	4	4	
Switch Phase							
Minimum Initial (s)	15.0		6.0		6.0	6.0	
Vlinimum Split (s)	20.0		9.1		11.0	11.0	
Total Split (s)	35.0	0.0	27.0	62.0	28.0	28.0	
Fotal Split (%)	38.9%	0.0%	30.0%	68.9%	31.1%	31.1%	
Maximum Green (s)	30.0		23.9		23.0	23.0	
Yellow Time (s)	3.0		3.0		3.0	3.0	
All-Red Time (s)	2.0		0.1		2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	5.0	4.0	3.1	3.1	5.0	5.0	
ead/Lag	Lag		Lead				
Lead-Lag Optimize?						annous and an extension	опшилить продрежения в сторой, а и с 2004 г. с месять опшили принципальный анти-
Vehicle Extension (s)	3.0		2.0		2.0	2.0	
Recall Mode	C-Max	e. · LUTE	None		None	None	A AND THE STATE OF
Act Effct Green (s)	44.7		71.9	75.6	9.1	9.1	
Actuated g/C Ratio	0.50		0.80	0.84	0.10	0.10	з веля сель том становиний принципання принципання принципання принципання принципання принципання принципання
//c Ratio	0.91		0.07	0.65	0.48	0.28	
Control Delay	41.5		7.1	12.5	46.6	13.5	
Queue Delay	0.0		0.0	0.3	0.0	0.0	a ang at ang
Total Delay	41.5		7.1	12.8	46.6	13.5	
LOS	D		A	12.0 B		В.	
LUG							
	41.5			12.5	,3.3		
Approach Delay Approach LOS	41.5 D			12.5 B	33.1 C		

	→	•	¥		7	<i>r</i>
Queue Length 95th (ft)	#857		m5	m182	91	35
Internal Link Dist (ft)	376			281	253	
Turn Bay Length (ft)			70			
Base Capacity (vph)	917		649	1565	452	449
Starvation Cap Reductn	0		0	127	0	0
Spillback Cap Reductn	0		0	0	0	3
Storage Cap Reductn	0		0	0	0	0
Reduced v/c Ratio	0.91		0.07	0.71	0.19	0.13

Other

Cycle Length: 90

Actuated Cycle Length: 90

Offset: 7 (8%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 70

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.91

Intersection Signal Delay: 25.8

leisection Signal Delay, 20.0

Intersection Capacity Utilization 62.0%

Intersection LOS: C

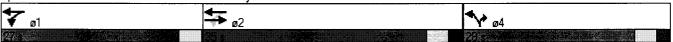
ICU Level of Service B

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

m Volume for 95th percentile queue is metered by upstream signal.



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Lane Configurations		414			44	7	*	^		ሻ	<u></u>	7
Volume (vph)	125	805	85	20	855	230	345	130	15	200	55	22 0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	11	11	13	11	11	16	11	13	13	11	11	13
Storage Length (ft)	0		125	0		2 5	230		0	300		300
Storage Lanes	0		1	0		1	1		0	1		1
Taper Length (ft)	25		25	25		25	25		25	25		25
Lane Util. Factor	0.95	0.95	0.95	0.95	0.95	1.00	1.00	1.00	1.00	1,00	1.00	1.0 0
Frt	m n n n milliollioùl e	0.987				0.850		0.985				0.850
Fit Protected		0.994			0.999		0.950			0.950		
Satd. Flow (prot)	0	3357	0	0	3418	1794	1711	1896	0	1711	1801	1636
Flt Permitted		0.522			0.901		0.573			0.657		
Satd. Flow (perm)	0	1763	0	0	3083	1794	1032	1896	0	1183	1801	1636
Right Turn on Red			Yes			Yes			No			No
Satd. Flow (RTOR)		14				54						
Link Speed (mph)		30			30	_		30			30	
Link Distance (ft)		209			822		. 11.2 1.1 1.1 1.1 1.1 1.1.	621			552	1
Travel Time (s)		4.8			18.7			14.1			12.5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	136	875	92	22	929	250	375	141	16	217	60	239
Shared Lane Traffic (%)					ii⊩Na ∓a						and a Second	
Lane Group Flow (vph)	0	1103	0	0	951	250	375	157	0	217	60	239
Turn Type	pm+pt			Perm		Prot	pm+pt			pm+pt		pt+ov
Protected Phases	1	12			2	2	3	8		7	4	41
Permitted Phases	12			2	2		8	8		4	4	
Detector Phase		12		2	2	2	3	8		7	4	4 1
Switch Phase							· · · · · · · · · · · · · · · · · · ·		47.101.111111111111111111111111111111111		ini in a sanat and a sanat and a sanat	
Minimum Initial (s)	6.0			15.0	15.0	15.0	6.0	6.0		6.0	6.0	
Minimum Split (s)	10.0	- 1,710[1710-1111 1471		20.5	20.5	20.5	10.0	10.9		10.0	10.9	
Total Split (s)	20.0	49.1	0.0	29.1	29.1	29.1	20.0	20.9	0.0	20.0	20 .9	40.9
Total Split (%)	22.2%	54.6%	0.0%	32.3%	32.3%	32.3%	22.2%	23.2%	0.0%	22.2%	23.2%	45.4%
Maximum Green (s)	16.0			23.6	23.6	23.6	16.0	16.0		16.0	16.0	
Yellow Time (s)	3.0			3.0	3.0	3.0	3.0	3.9		3.0	3.9	
All-Red Time (s)	1.0			2.5	2.5	2.5	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	4.0	4.0	4.0	5.5	5.5	5.5	4.0	4.9	4.0	4.0	4.9	4.9
Lead/Lag	Lead			Lag	Lag	Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize?				Luy	Luy			_~9				
Vehicle Extension (s)	0.2			0.2	0.2	0.2	2.0	2.0		2.0	2.0	
Recall Mode	Max			C-Max	C-Max	C-Max	None	None None		None	None	
Act Effct Green (s)		44.4		- Ulium	23.6	23.6	32.3	16.4		26.3	13.1	36.4
Actuated g/C Ratio		0.49			0.26	0.26	0.36	0.18	14:12: 210: 211	0.29	0.15	0.40
v/c Ratio		0.90			1.18	0.49	0.77	0.46		0.52	0.23	0.36
Control Delay		28.2			124.3	25.6	34.6	37.5		24.6	34.9	20.9
Queue Delay		0.0			0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay		28.2			124.3	25.6	34.6	37.5		24.6	34.9	20.9
LOS		20.2 C			124.0 F	20.0 C	- 34.0 C	- 07.0 D		24. 0	. 34.5 C	20.9 C
Approach Delay		28.2			103.8			35.5		U	24.1	
			7 374									
Approach LOS		С			F			D			С	

	۶	-	*	•	←	•	4	†	-	-	↓	4
											4.4	. 124%
Queue Length 50th (ft)		169			-344	93	165	79		85	30	93
Queue Length 95th (ft)		#326			#465	166	#259	141		135	65	154
Internal Link Dist (ft)		129			742			541			472	
Turn Bay Length (ft)						25	230			300		300
Base Capacity (vph)		1219			808	510	491	353		488	320	651
Starvation Cap Reductn		0			0	0	0	0		0	0	C
Spillback Cap Reductn		0			0	0	0	0		0	0	0
Storage Cap Reductn		0			0	0	0	0		0	0	0
Reduced v/c Ratio		0.90			1.18	0.49	0.76	0.44		0.44	0.19	0.37

Other

Cycle Length: 90

A CONTRACTOR OF THE CONTRACTOR

Actuated Cycle Length: 90

Offset: 46 (51%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 65

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.18
Intersection Signal Delay: 55.8

Intersection Capacity Utilization 92.3%

Intersection LOS: E
ICU Level of Service F

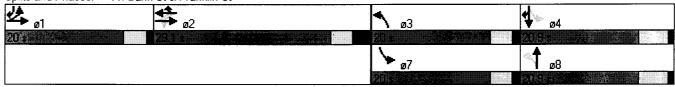
Analysis Period (min) 15

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 11: Bank St & Franklin St



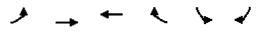
	→	•	1	←	4	<i>*</i>
Personal Communication Communi						
Lane Configurations	F)			ની	¥	
Volume (veh/h)	725	40	160	990	0	165
Sign Control	Free			Free	Stop	
Grade	0%	0.00	0.00	0%	0%	0.00
Peak Hour Factor	0.92 788	0.92 43	0.92 174	0.92 1076	0.92 0	0.92 179
Hourly flow rate (vph) Pedestrians	100		1/4	1070	Y.	
Lane Width (ft)				neer ligen		
Walking Speed (ft/s)						
Percent Blockage						
Right turn flare (veh)					" allulud quanu	
Median type	None			None		
Median storage veh)						
Upstream signal (ft)	361			275		
pX, platoon unblocked			0.56		0.71	0.56
vC, conflicting volume			832		2234	810
vC1, stage 1 conf vol						
vC2, stage 2 conf vol			202		4422	264
vCu, unblocked vol tC, single (s)	git reen.	n en ja	303 4.1		1133 6.4	6.2
tC, 2 stage (s)			7.		0.4	
tF (s)			2.2	1-12 Webi	3.5	3.3
p0 queue free %			75	-11 -41 -161-161	100	59
cM capacity (veh/h)			702	aranyanidi Salah	119	432
Alfationales in the						
Volume Total	832	1250	179			BEWIN CONTRACTOR OF THE STREET
Volume Left	0	174	0			
Volume Right	43	0	179			
cSH	1700	702	432			an more a community of the second more annual more and the second more and the second more and the second more annual
Volume to Capacity	0.49	0.25	0.41			
Queue Length 95th (ft)	0	24	50		e e e catani	ndontranta de la calca altre calculation de la minima de crimo éléctro de la colonidad de la colonidad de la c
Control Delay (s) Lane LOS	0.0	8.5	19.1			
Lane LOS Approach Delay (s)	0.0	A 8.5	C 19.1	elastaja.		
Approach LOS	0.0	0.0				
rio de la companya de						
Average Delay			6.2			
Intersection Capacity Utilizati	on		121.7%	le)	U Level d	of Service H
Analysis Period (min)			15			
	o de establicación en e					

Right turn flare (veh) Median type		-	*	•	←	1	<i>*</i>	
Volume (veh/h) 910 40 155 1125 20 90 Sign Control Free Free Stop Grade 0 0% 0% 0% Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 Free Stop Free Stop Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 Free Stop Free Stop Free Stop Owk 0% Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 Free Stop Free Stop Free Stop Free Stop Owk 0% Peak Hour Factor 0.92 0.92 0.92 0.92 Free Stop Free Stop Owk 0% Peak Hour Factor 0.92 0.92 0.92 0.92 Free Stop Free Stop Owk 0% Peak Hour Factor Owk 0% Peak Hour Factor Owk 09% Ow	Manager							
Sign Control Free			ti edinine s ga nisi.	ሻ	<u>†</u>			
Grade 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0%			40	155			*** 90	
Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92			r i geletgelagaja					
Hourly flow rate (vph) 989 43 168 1223 22 98 Pedestrians Jane Width (ft) Walking Speed (ft/s) Percent Blockage Right run flare (veh) Median type Median type Median storage veh) Jpstream signal (ft) 175 1318 Jpstream signal (ft) 175 1318 Jpstream signal (ft) 175 1011 KC, platoon unblocked JC, conflicting volume 1033 2571 1011 CC2, stage 1 conf vol JC2, stage 2 conf vol JC2, stage (s) JC, stage (s) JC, stage (s) JC, 2 stage (s) JC, 3 stage (s) JC, 4 stage (0 02	0 02			0 Q2	
Pedestrians ane Width (ft) Walking Speed (ft/s) Percent Blockage Right turn flare (veh) Median type None Median storage veh) Upstream signal (ft) 175 1318 100, platoon unblocked CC, conflicting volume CC, stage 2 conf vol CC, stage 2 conf vol CC, stage 2 conf vol CC, stage (s) CC, 2 stage (s) F (s) 100, platoon unblocked CC, 2 stage (s) CF (s) 101 102 103 104 105 105 106 107 107 107 107 107 107 107								
Cane Width (ft) Canada C					1.447	ya uu ha o		
Valking Speed (ft/s) Percent Blockage Right turn flare (veh) Wedian storage veh) Upstream signal (ft) 175 1318 Jpstream signal (ft) 175 1318 0.72 0.74 XC, palloton unblocked 0.74 0.72 0.74 VC, conflicting volume 1033 2571 1011 VC1, stage 1 conf vol VC2, stage 2 conf vol VC2, stage 2 conf vol 4.1 6.4 6.2 C, 2 stage (s) 4.1 6.4 6.2 C, 2 stage (s) 7.1 14 64 MC capacity (veh/h) 576 25 271 Stant (veh/h) 576 22 22 Volume Left 0 168 0 22 Volume Left 0 168 0 29 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
Percent Blockage Right turn flare (veh) Median type								
Median type None None Median storage veh) Jpstream signal (ft) 175 1318 Jx, platoon unblocked 0.74 0.72 0.74 JCD, conflicting volume 1033 2571 1011 JCD, stage 1 conf vol JCD, stage 2 conf vol 2192 843 JCD, single (s) 4.1 6.4 6.2 JC, 2 stage (s) 5F (s) 3.5 3.3 JO queue free % 71 14 64 Mcdacatity (veh/h) 576 25 271 JBLB JOUING Total 1033 168 1223 120 Volume Left 0 168 0 22 Volume Right 43 0 0 98 CSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 1.7 243.3 Approa	Percent Blockage						(1) (2) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	
Median storage veh) Jpstream signal (ft) 175 1318 DX, platoon unblocked vC, conflicting volume vC1, stage 1 conf vol 1033 2571 1011 VC2, stage 1 conf vol vC2, stage 2 conf vol vC2, stage (s) 872 2192 843 C, single (s) 4.1 6.4 6.2 6.2 C, 2 stage (s) 71 14 64 SM capacity (veh/h) 576 25 271 SM capacity (veh/h) 576 25 271 SM capacity (veh/h) 576 25 271 SH 100 98 Volume Right 43 0 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 1.8 0.0 243.3 Jane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F	Right turn flare (veh)							
Jostream signal (ft) 175	Median type	None			None			
DX, platoon unblocked OC, conflicting volume 1033 2571 1011 CCI, stage 1 conf vol CCI, stage 2 conf vol CCI, unblocked vol CCI, single (s) CC, 2 stage (s) F (s) D0 queue free % T1 14 64 M capacity (veh/h) T68 O 168 O 22 Volume Total Volume Right 43 O 0 98 DSH 1700 576 1700 98 DO 172 Dueue Length 95th (ft) O 30 O 205 Control Delay (s) D0 17 D4 D4 D5 D6 D6 D7 D7 D7 D8 D8 D8 D9 D9 D9 D9 D9 D9 D9							enemental social control of capa 5 . At resident termination and the AV 2 . The STATE STREET Co. Se	a adoron Si
/C, conflicting volume /C1, stage 1 conf vol /C2, stage 2 conf vol /C2, stage 2 conf vol /C3, stage 2 conf vol /C4, stage 2 conf vol /C5, stage (s) /C5, stage (s) /C6, stage (s) /C7, stage (s) /C7, stage (s) /C8, stage (s) /C9, sta	- · · · · · · · · · · · · · · · · · · ·	175			1318			
/C1, stage 1 conf vol //C2, stage 2 conf vol //C3, stage 2 conf vol //C4, unblocked vol 872 2192 843 C5, single (s) 4.1 6.4 6.2 C7, 2 stage (s) F (s) 2.2 3.5 3.3 D0 queue free % 71 14 64 DM capacity (veh/h) 576 25 271 DVolume Total 1033 168 1223 120 Volume Left 0 168 0 22 Volume Right 43 0 0 98 SSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach LOS F		10000						
/CQ, stage 2 conf vol /Cu, unblocked vol 872 2192 843 C, single (s) 4.1 6.4 6.2 C, 2 stage (s) F (s) 2.2 3.5 3.3 Ø queue free % 71 14 64 M capacity (veh/h) 576 25 271 Olume Total 1033 168 1223 120 Volume Left 0 168 0 22 Volume Right 43 0 0 98 SSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 a.ane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach Delay (s) 0.0 1.7 243.3 Approach LOS F				1033		25/1		
/Cu, unblocked vol 872 2192 843 /C, single (s) 4.1 6.4 6.2 C, 2 stage (s) F (s) 2.2 3.5 3.3 00 queue free % 71 14 64 M capacity (veh/h) 576 25 271 // Olume Total 1033 168 1223 120 // Olume Left 0 168 0 22 // Olume Right 43 0 0 98 CSH 1700 576 1700 98 // Olume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 _ane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach Delay (s) 0.0 1.7 243.3 Approach LOS F								
C, single (s) C, 2 stage (s) F (s) C, 3 stage (s) F (s) C, 2 stage (s) F (s) C, 3 stage (s) F (s) C, 2 stage (s) F (s) C, 3 stage (s) F (s) C, 2 stage (s) F (s) C, 3 stage (s) F (s) C, 4 stage (s) F (s) C, 5 stage (s) F (s) C, 4 stage (s) F (s) C, 5 stage (s) F (s) C, 6 stage (s) F (s) C, 6 stage (s) F (s) C, 7 stage (s) F (s) C, 8 stage (s) F (s) C, 9 stage (s) F (s) C, 1 stage (s) F (s) C, 2 stage (s) F (s) C, 3 stage (s) F (s) C, 2 stage (s) F (s) C, 2 stage (s) F (s) C, 2 stage (s) F (s) C, 3 stage (s) F (s) C, 2 stage (s) F (s) C, 3 stage (s) F (s) C, 4 stage (s) F (s) C, 5 stage (s) F				872		2102	843	
C, 2 stage (s) F (s)								
## Second Compact Comp								
71 14 64 cM capacity (veh/h) 576 25 271 Volume Total 1033 168 1223 120 Volume Left 0 168 0 22 Volume Right 43 0 0 98 cSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F				2.2		3.5	3.3	
Volume Total 1033 168 1223 120 Volume Left 0 168 0 22 Volume Right 43 0 0 98 CSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F	o0 queue free %			71		14	64	
Volume Total 1033 168 1223 120 Volume Left 0 168 0 22 Volume Right 43 0 0 98 cSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F	cM capacity (veh/h)			576		25	271	
Volume Left 0 168 0 22 Volume Right 43 0 0 98 CSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F	Allesta dalla							
Volume Right 43 0 0 98 cSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F	AND THE PROPERTY OF THE PROPER						The state of the s	
SSH 1700 576 1700 98 Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F	and the second of the second o							s holdhi s
Volume to Capacity 0.61 0.29 0.72 1.22 Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F								
Queue Length 95th (ft) 0 30 0 205 Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F								
Control Delay (s) 0.0 13.8 0.0 243.3 Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F								
Lane LOS B F Approach Delay (s) 0.0 1.7 243.3 Approach LOS F								
Approach Delay (s) 0.0 1.7 243.3 Approach LOS F	_ane LOS						in an	
Average Delay 12.4	Approach Delay (s)	0.0			243.3			
Average Delay 12.4	Note that the second se							
	Average Delay			12.4				

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Lane Configurations	۲	†	1>			
Volume (veh/h)	5	1000	1280	95	0	0
Sign Control	ent e indomblektion	Free	Free	te o di addes c	Stop	
Grade	0.00	0%	0%	0.00	0%	0.00
Peak Hour Factor Hourly flow rate (vph)	0.92 5	0.92 1087	0.92 1391	0.92 103	0.92 0	0.92 0
Pedestrians		1007	1991	100		
Lane Width (ft)						
Walking Speed (ft/s)						indiandalimineralimine (A.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C
Percent Blockage		ldbl.:				· · · · · · · · · · · · · · · · · · ·
Right turn flare (veh)						
Median type		None	None			
Median storage veh)		640	004			
Upstream signal (ft) pX, platoon unblocked	0.52	612	881		0.67	0.52
vC, conflicting volume	1495				2541	1443
vC1, stage 1 conf vol			· · · · · · · · · · · · · · · · · · ·			The Mark Mark Control of the Control
vC2, stage 2 conf vol						Andrew Control of the
vCu, unblocked vol	1490				2070	1391
tC, single (s)	4.1				6.4	6.2
tC, 2 stage (s)		NETS CONSTRUCTION	14 - ESBART AN			
tF (s)	2.2 98	FARRY.			3.5 100	3.3 100
p0 queue free % cM capacity (veh/h)	236				39	91
Civi capacity (verimi)		55.000.4F1			- 33	31 31 Example 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Volume Total	5	1087	1495			
Volume Left	5	0	0			HE (1331), 166, Mai V. V. (1444),
Volume Right	0	0	103			
cSH	236	1700	1700			
Volume to Capacity	0.02	0.64	0.88			
Queue Length 95th (ft)	2	0	0 0.0			STANTON (S. C. S. C. STANTS STANTS STANTS SANTON STANTS STANTS STANTS STANTS STANTS STANTS STANTS STANTS STANTS
Control Delay (s) Lane LOS	20.6 C	0.0	0.0			
Approach Delay (s) Approach LOS	0.1	7.5,8 .0	0.0			
Average Delay			0.0			
			U.U			
Intersection Capacity Utiliza	ation		76.5%	IC.	U Level o	of Service D
Intersection Capacity Utiliza Analysis Period (min)	ation				U Level o	of Service D

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Lane Configurations	ሻ	†	1}•		¥	
Volume (vph)	20	775	610	5	80	25
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (ft)	100			0	0	0
Storage Lanes	1			0	1	0
Taper Length (ft)	25	11.1. a.141.00 a.100		25	25	25
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fit			0.999		0.968	
FIt Protected	0.950				0.963	
Satd. Flow (prot)	1770	1863	1861	. 0	1736	
Flt Permitted	0.314				0.963	
Satd. Flow (perm)	585	1863	1861	0	1736	0
Right Turn on Red				No		No
Satd. Flow (RTOR)						
Link Speed (mph)		3 0	30		30	
Link Distance (ft)		275	175		403	
Travel Time (s)		6.3	4.0		9.2	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	22	842	663	5	87	27
Shared Lane Traffic (%)						
Lane Group Flow (vph)	22	842	668	0	114	0
Turn Type	pm+pt					
Protected Phases	1	1 2	2		4	·
Permitted Phases	12	2				
Detector Phase	1	1 2	2		4	
Switch Phase						
Minimum Initial (s)	3.0		15.0		7.0	
Minimum Split (s)	6.1		20.0		11.0	
Total Split (s)	8.1	62.0	53.9	0.0	18.0	0.0
Total Split (%)	10.1%	77.5%	67.4%	0.0%	22.5%	0.0%
Maximum Green (s)	5.0		48.9		14.0	
Yellow Time (s)	3.0		3.0		3.0	
All-Red Time (s)	0.1		2.0		1.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	3.1	3.1	5.0	4.0	4.0	4.0
Lead/Lag	Lead		Lag			
Lead-Lag Optimize?						
Vehicle Extension (s)	1.5		5.0		1.5	
Recall Mode	None	2.72	C-Min		None	A production of the control of the c
Act Effct Green (s)	62.5	66.2	51.8		9.5	
Actuated g/C Ratio	0.78	0.83	0.65		0.12	TON TON THE REPORT OF THE CONTROL OF THE CONTROL OF THE PROPERTY OF THE PROPER
v/c Ratio	0.04	0.55	0.55		0.55	
Control Delay	2.8	4.3	8.8		42.8	
Queue Delay	0,0	0.0	0.0		0.0	
Total Delay	2.8	4.3	8.8		42.8	
LOS	Α	A	A		D	
Approach Delay		4.3	8.8	onma ausanna in	42.8	
Approach LOS		Α	Α		D	
Queue Length 50th (ft)	2	109	98		55	



Queue Lenath 95th (ft)	m5	185	128	100
Internal Link Dist (ft)		195	95	323
Turn Ray Length (ft)	100			
Base Capacity (vph)	586	1555	12 20	304
Starvation Cap Reductn	0	49	0	0
Spillback Cap Reductn	0	0	0	0
Storage Cap Reductn	0	0	. 0	0
Reduced v/c Ratio	0.04	0.56	0.55	0.38

Other

Cycle Length: 80

Actuated Cycle Length: 80

Offset: 1 (1%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.55

Intersection Signal Delay: 8.8

Intersection LOS: A

Intersection Capacity Utilization 53.4%

ICU Level of Service A

Analysis Period (min) 15

m Volume for 95th percentile queue is metered by upstream signal.

Splits and Phases: 2: Bank St & Old Dr (west)



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E			<u>-</u>			
Lane Configurations	f		ሻ	†	ሻ	7
Volume (vph)	690	80	35	515	35	35
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (ft)	1000	0	70		0	0
Storage Lanes		0	1		1	1
Taper Length (ft)		25	25		25	25
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
	0.986	1.00	1.00	1.00	1.00	0.850
Ti Destadad	0.900		0.0E0		0 0E0	U.OOU
Fit Protected	4007		0.950	4000	0.950	4500
Satd, Flow (prot)	1837	0	1770	1863	1770	1583
FIt Permitted		·····	0.248		0.950	
Satd. Flow (perm)	1837	0	462	1863	1770	1583
Right Turn on Red		Yes	1			Yes
Satd. Flow (RTOR)	15					38
Link Speed (mph)	30			30	30	
Link Distance (ft)	456			361	333	
Travel Time (s)	10.4			8.2	7.6	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	750	87	38	560	38	38
Shared Lane Traffic (%)						
Lane Group Flow (vph)	837	0	38	560	38	38
Turn Type			pm+pt			Prot
Protected Phases	2		1	1 2	4	4
Permitted Phases			12	2	4	
Detector Phase	2		1	12	4	4
Switch Phase				1 4 :::::::::::::::::::::::::::::::::::		7
	450	: Edda		ia de dala	60	60
Minimum Initial (s)	15.0		6.0		6.0	6.0
Minimum Split (s)	20.0		9.1	A- A	11.0	11.0
Total Split (s)	56.9	0.0	10.1	67.0	13.0	13.0
Total Split (%)	71.1%	0.0%	12.6%	83.8%	16.3%	16.3%
Maximum Green (s)	51.9		7.0		8.0	8.0
Yellow Time (s)	3.0		3.0		3.0	3.0
All-Red Time (s)	2.0		0.1		2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	5.0	4.0	3.1	3.1	5.0	5.0
Lead/Lag	Lag		Lead			
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0		2.0		2.0	2.0
Recall Mode	C-Max		None		None	None
Act Effct Green (s)	57.5		66.5	70.9	6.7	6.7
Actuated g/C Ratio	0.72	# ####################################	0.83	0.89	0.08	0.08
v/c Ratio	0.63		0.08	0.34	0.26	0.23
Control Delay	9.9		0.00	1.0	38.5	15.4
Queue Delay	0.0		0.0	0.0	0.0	0.0
Total Delay	9.9		0.9	1.0	38.5	15.4
LOS	A		A	A	D	В
Approach Delay	9.9			1.0	26.9	
Approach LOS	A			A	C	
Queue Length 50th (ft)	231		1	16	18	0

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: +					
Queue Length 95th (ft)	362	m2	21	46	27
Internal Link Dist (ft)	376		281	253	
Turn Bay Length (ft)	ogallikiS	70			
Base Capacity (vph)	1325	509	1631	177	193
Starvation Cap Reductn	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0
Storage Cap Reductn		0	0	. 0	0
Reduced v/c Ratio	0.63	0.07	0.34	0.21	0.20

Other

Cycle Length: 80

Actuated Cycle Length: 80

Offset: 7 (9%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.63

Intersection Signal Delay: 7.3

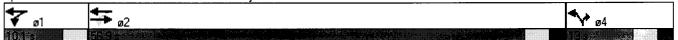
Intersection LOS: A

Intersection Capacity Utilization 54.5%

ICU Level of Service A

Analysis Period (min) 15

m Volume for 95th percentile queue is metered by upstream signal.



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												:) + 3 × .
Lane Configurations		414			4₽	7	ሻ	(أ		ሻ	†	7
Volume (vph)	95	740	85	10	520	80	140	20	10	80	25	50
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	11	11	13	11	11	16	11	13	13	11	11	13
Storage Length (ft)	0		125	0	-000	25	230	''-: -::::	0	300	P*************************************	300
Storage Lanes	0		1	Ō		1	1		0			1
Taper Length (ft)	25		25	25	lese to seconds.	25	25		25	25		25
Lane Util. Factor	0.95	0.95	0.95	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt	· · · · · · · · · · · · · · · · · · ·	0.986	da di IV NY MAIN			0.850		0.950				0.850
Fit Protected		0.995			0.999		0.950	0,000		0.950		
Satd. Flow (prot)	0	3356	0	0	3418	1794	1711	1829	0	1711	1801	1636
Fit Permitted		0.836			0.929	1707	0.833	1020		0.606		
Satd. Flow (perm)	0	2820	0	0	3178	1794	1500	1829	0	1091	1801	1636
Right Turn on Red	U	2020	Yes		3170	Yes	1300	1023	No.	1001	1001	No
		22	i es			43			UNU			
Satd. Flow (RTOR)	. Chi. I magazini					43		30			30	gra tele
Link Speed (mph)	578 7850 3534 Jabb 18 1922 5	30			30			621			552	
Link Distance (ft)	e a contentialistición	209			822							
Travel Time (s)		4.8	^ ^^	0.00	18.7	^ ^^	^ ^^	14.1	0.00	^ ^^	12.5	0.00
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	103	804	92	11	565	87	152	22	11	87	27	54
Shared Lane Traffic (%)			mana nangipulas	t			erekananga <u>ngga</u> an	an ann meete var	11 mm - 56, 2145			
Lane Group Flow (vph)	0	999	0	0	576	87	152	33	0	87	27	54
Turn Type	pm+pt			Perm		Prot	pm+pt			pm+pt	and the second of	pt+ov
Protected Phases	1	12			2	2	3	8		7	4	41
Permitted Phases	1 2			2	2		8	8		4	4	
Detector Phase	1.	1 2		2	2	2	3	8		7	4	41
Switch Phase												
Minimum Initial (s)	6.0			15.0	15.0	15.0	6.0	6.0		6.0	6.0	
Minimum Split (s)	10.0			20.5	20.5	20.5	10.0	10.9		10.0	10.9	
Total Split (s)	17.0	54.0	0.0	37.0	37.0	37.0	15.0	14.0	0.0	12.0	11.0	28.0
Total Split (%)	21.3%	67.5%	0.0%	46.3%	46.3%	46.3%	18.8%	17.5%	0.0%	15.0%	13.8%	35.0%
Maximum Green (s)	13.0			31.5	31.5	31.5	11.0	9.1		8.0	6.1	
Yellow Time (s)	3.0			3.0	3.0	3.0	3.0	3.9		3.0	3.9	
All-Red Time (s)	1.0			2.5	2.5	2.5	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	4.0	4.0	4.0	5.5	5.5	5.5	4.0	4.9	4.0	4.0	4.9	4,9
Lead/Lag	Lead			Lag	Lag	Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize?												
Vehicle Extension (s)	0.2			0.2	0.2	0.2	2.0	2.0		2.0	2.0	
Recall Mode	Max			C-Max	C-Max	C-Max	None	None		None	None	
Act Effct Green (s)		49.3			31.5	31.5	13.9	7.2		15.7	6.1	24.3
Actuated g/C Ratio		0.62		Rational Land	0.39	0.39	0.17	0.09		0.20	0.08	0.30
v/c Ratio		0.54			0.46	0.12	0.53	0.20		0.28	0.20	0.11
Control Delay		7.1			19.5	9.4	34.7	35.9	Page 15, 175, 111, 50007-111,	25.4	38.4	21.7
Queue Delay	etracht e (457 f	0.0	ar seressan en c	A COSSISSION	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay		7.1			19.5	9.4	34.7	35.9		25.4	38.4	21.7
LOS	. 111 / 121				·····		C	D		20. 4 C	30. 4 D	21.7 C
	-1 -1 Land 3 ¹ :	A 74			B 404	Α		34.9			26 .3	
Approach Delay		7.1			18.1							
Approach LOS		Α			В			С			С	

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										31	:\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
Queue Length 50th (ft)	76			109	13	73	16		33	13	20
Queue Length 95th (ft)	120			154	41	110	41		69	37	47
Internal Link Dist (ft)	129			742			541			472	
Turn Bay Length (ft)					25	230			300		300
Base Capacity (vph)	1856			1251	732	310	208		323	137	476
Starvation Cap Reductn	0			0	0	0	0		0	0	0
Spillback Cap Reductn	0			0	0	0	0		0	0	0
Storage Cap Reductn	0			0	0	0	0		0	0	0
Reduced v/c Ratio	0.54			0.46	0.12	0.49	0.16		0.27	0.20	0.11

Other

Cycle Length: 80

Actuated Cycle Length: 80

Offset: 46 (58%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 55

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.54

Intersection Signal Delay: 14.9

Intersection Capacity Utilization 67.0%

Analysis Period (min) 15

Intersection LOS: B

ICU Level of Service C

Splits and Phases: 11: Bank St & Franklin St



	→	\rightarrow	•	←	•	<i>></i>				
April 1944										
Lane Configurations	f			र्स	¥¥					
Volume (veh/h)	690	30	70	555	5	90				
Sign Control	Free	e en invasiones e		Free	Stop				emmanananan ilikanga 1969g, da	
Grade	0%			0%	0%					
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92				1954
Hourly flow rate (vph)	750	33	76	603	5	98				
Pedestrians Lane Width (ft)			residencia (com							
Walking Speed (ft/s)										
Percent Blockage										
Right turn flare (veh)										
Median type	None			None						
Median storage veh)										
Upstream signal (ft)	361	ello el		275						
pX, platoon unblocked			0.73		0.84	0.73				
vC, conflicting volume			783		1522	766				
vC1, stage 1 conf vol								· · · · · · · · · · · · · · · · · · ·	none and an annual contraction of the second second	
vC2, stage 2 conf vol										
vCu, unblocked vol			518		946	496		925.6.3.46.586.558655866		
tC, single (s)			4.1		6.4	6.2				
tC, 2 stage (s)			2.2		25	3.3	CASSACTAR CARAGOSTINA		Abel Matribosa , Testillinin s. Habi	
tF (s) p0 queue free %			90		3.5 98	3.3 77				
cM capacity (veh/h)	Herodonialise d		766		219	419				
					- /Y					Per d
Volume Total	783	C70	400					•		
Volume Left	763	679 76	103							
Volume Right	33	0	5 98							
cSH	1700	766	400		karian ee i					3.15
Volume to Capacity	0.46	0.10	0.26							
Queue Length 95th (ft)	0	8	25				i -1.330.3.330.300.000			
Control Delay (s)	0.0	2.5	17.1							
Lane LOS	M-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	Α	С	. To come not to be to be to be	a salverative					
Approach Delay (s)	0.0	2.5	17.1							
Approach LOS			C							
A Commence of the Commence of										
Average Delay			2.2							
Intersection Capacity Utiliza	tion		87.1%	IC	U Level o	of Service		E		
Analysis Period (min)			15		- actions					

	→	\rightarrow	•	←		<i>*</i>
ane Configurations	₽		ካ	A	ኻ	7
/olume (veh/h)	825	30	80	_595 _	_ 16	90.
Sign Control	Free			Free	Stop	
Grade	0%	0.92	0.00	0% 0.92	0% 0.92	0.92
Peak Hour Factor Hourly flow rate (vph)	0.92 897	0.92 33	0.92 87	647	0.92 - 17	0.92 98
Pedestrians	001			- VT/-	i de la constitución	
ane Width (ft)						
Valking Speed (ft/s)						
Percent Blockage						
Right turn flare (veh)					ness se si motor cri	
Median type	None			None		
Median storage veh)	475			1318		
Jpstream signal (ft) DX, platoon unblocked	175		0.80	1310	0.89	0.80
C, conflicting volume			929		1734	913
C1, stage 1 conf vol			YEY			
C2, stage 2 conf vol						""一个看来,""一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个
Cu, unblocked vol			785		1297	765
C, single (s)			4.1		6.4	6.2
C, 2 stage (s)		uan in Hebritania				
F (s)			2.2		3. 5 87	3.3
o0 queue free % cM capacity (veh/h)			87 665		07 138	70 322
ovi capacity (verim)			000		190	
Volume Total	929	87	647	17	98	
/olume Left	0	87	0	17	0	· Control of the state of the s
/olume Right	33	0	0	0	98	
SH	1700	665	1700	138	322	Communication (Communication of Communication Communication (Communication Communication Communication Com
/olume to Capacity	0,55	0.13	0.38	0.13	0.30	
Queue Length 95th (ft)	0	11	0	11	31	「Town Constitution Commitment A 表をおうというできません When the machine in the contribution にいく 中国の大阪の国際の公司
Control Delay (s) Lane LOS	0.0	11.2 B	0.0	34.8 D	21.0 C	
Approach Delay (s)	00					
Approach LOS		1,0		C		Comment of the property of Approximated Appr
- Marketa						
Average Delay			2.0			
ntersection Capacity Utiliz	zation		63.0%	IC	U Level o	of Service B
Analysis Period (min)		dalland dagan in Andreid	15			

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Stephen C										
Lane Configurations	'n	1	î,				•			<u> </u>
Volume (veh/h)	5	915	670	25	0	0				
Sign Control		Free	Free		Stop					
Grade		0%	0%		0%					
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92		:	grappe i - Nobelessesses	
Hourly flow rate (vph)	. 5	995	728	27	0	0				
Pedestrians	, en come escape a programme.		ve tiese, averon	es esteriores se etc.	Tala sapagitas sõ	gaesquest to les electronia	easte ann in imit			
Lane Width (ft)		Anidata,								
Walking Speed (ft/s)										
Percent Blockage										
Right turn flare (veh) Median type		None	None							
Median storage veh)		INONG	NUILE							
Upstream signal (ft)		612	881							
pX, platoon unblocked	0.77				0.88	0.77		Test		TRACERIBLES COMMENTS OF STREET
vC, conflicting volume	755	er leggest legjest. Et lauter alle			1747	742				
vC1, stage 1 conf vol		*** *** **** ***							P	. , , ,
vC2, stage 2 conf vol										
vCu, unblocked vol	530				1215	512				
tC, single (s)	4.1				6.4	6.2				
tC, 2 stage (s)										and to seem to the seem of an artist
tF (s)	2.2				3.5	3.3				
p0 queue free %	99				100	100				STATE THE HILLING HE C. D. C
cM capacity (veh/h)	796				175	431				
Volume Total	5	995	755							
Volume Left	5	0	0							384 p. 123 (1990)
Volume Right	0	o o	27							
cSH	796	1700	1700	er, ngalladadida.						Aar B. C Down Hill Hilling of Hill
Volume to Capacity	0.01	0.59	0.44			Allia deition				
Queue Length 95th (ft)	1	0	0				e, print estimation			
Control Delay (s)	9.6	0.0	0.0		tribili					
Lane LOS	Α									
Approach Delay (s) Approach LOS	0.1		0.0							
(State of the										
Average Delay			0.0							
Intersection Capacity Util	ization		51.5%	IC	U Level c	f Service		A		
Analysis Period (min)	neve eneme enemikiii		15							

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: •						
Lane Configurations	ሻ		1>		¥f	
Volume (vph)	40	880	1140	5	70	35
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (ft)	100			. 0	0	0
Storage Lanes	1			0	1	0
Taper Length (ft)	25			25	25	25
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	1000 mg		0.999		0.955	
Flt Protected	0.950				0.968	
Satd. Flow (prot)	1770	1863	1861	0	1722	0
Flt Permitted	0.103	000000000000000000000000000000000000000	arminati Sutanti da	e de la distribución de la constantida	0.968	
Satd. Flow (perm)	192	1863	1861	0	1722	0
Right Turn on Red	d padite ipjedulkokomomie		· · · · · · · · · · · · · · · · · · ·	No		No
Satd. Flow (RTOR)				_		
Link Speed (mph)		30	30		30	
Link Distance (ft)		275	175		403	
Travel Time (s)		6.3	4.0		9.2	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	43	957	1239	5	76	38
Shared Lane Traffic (%)						
Lane Group Flow (vph)	43	957	1244	0	114	0
Turn Type	pm+pt					
Protected Phases	1	12	2		4	
Permitted Phases	12	2				
Detector Phase	1	12	2		4	. (Claima 1964 1966 — 1964 г. (Укадана) учина принципания принципания (ССС) (ССС) (ССС) (ССС) (ССС) (ССС) (ССС)
Switch Phase						
Minimum Initial (s)	3.0		15 .0		7.0	
Minimum Split (s)	6.1		20.0		11.0	
Total Split (s)	5.1	48.1	43.0	0.0	11.9	0.0
Total Split (%)	8.5%	80.2%	71.7%	0.0%	19.8%	0.0%
Maximum Green (s)	2.0		38.0		7.9	
Yellow Time (s)	3.0		3.0		3.0	
All-Red Time (s)	0.1		2.0		1.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	3.1	3.1	5.0	4.0	4.0	4.0
Lead/Lag	Lead	potential Programmes	Lag			
Lead-Lag Optimize?						
Vehicle Extension (s)	1.5	e Herri	5.0		1.5	
Recall Mode	None		C-Min		None	
Act Effct Green (s)	44.5	48.2	39.7		7.5	
Actuated g/C Ratio	0.74	0.80	0.66		0.12	
v/c Ratio	0.20	0.64	1.01		0.53	
Control Delay	4.0	4.8	43.3		34.0	
Queue Delay	0.0	0.0	0.0		0.0	
Total Delay	4.0	4.8	43.3		34.0	
LOS	Α	Α	D		С	en di Bargore dell'esse dell'altre e primitatione dell'esse dell'esse dell'esse dell'esse dell'esse dell'esse
Approach Delay		4.7	43.3		34.0	
Approach LOS		A	D.		С	
Queue Length 50th (ft)	3	90	~510		39	

<u>ر</u>	→	4	4	1	1
				-	•

Queue Length 95th (ft)	m7	184	#728	83
Internal Link Dist (ft)		195	95	323
Turn Bay Length (ft)	100			
Base Capacity (vph)	219	1496	1230	227
Starvation Cap Reductn	0	3	0	0
Spillback Cap Reductn	0	0	0	0
Storage Cap Reductn	0	0		
Reduced v/c Ratio	0.20	0.64	1.01	0.50

Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 90

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.01

Intersection Signal Delay: 26.5

Intersection Capacity Utilization 73.8%

Intersection LOS: C

ICU Level of Service D

Analysis Period (min) 15

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

- # 95th percentile volume exceeds capacity, queue may be longer.

 Queue shown is maximum after two cycles.
- m Volume for 95th percentile queue is metered by upstream signal.

Splits and Phases: 2: Bank St & Old Dr (west)



	-	•	<	←	4	1	
·. ·				1,1			
ane Configurations	ĵ»		ሻ	↑	ሻ	7	
/olume (vph)	705	60	40	940	80	55	
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (ft)		0	70		Ö	0	
Storage Lanes		0	1		1	1	
aper Length (ft)	e digitaliy	25	25		25	25	
ane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	New York and the control of the cont
rt	0.989				+ 1111111	0.850	
It Protected	0.000		0.950		0.950		
Satd. Flow (prot)	1842	0	1770	1863	1770	1583	Marchaelle (Marchaelle Marchaelle Marchaelle Marchaelle Marchaelle Marchaelle Marchaelle Marchaelle Marchaelle
It Permitted	1072	· · · · · · · · · · · · · · · · · · ·	0.222	1000	0.950		
	1842	0	414	1863	1770	1583	**************************************
Satd. Flow (perm)	1042		414	1000	1770		
Right Turn on Red		Yes				Yes	
Satd. Flow (RTOR)	13					60	
ink Speed (mph)	30	Michaelan i m	and the second	30	30		
ink Distance (ft)	456			361	333		
ravel Time (s)	10.4	nor arabbancanta		8.2	7.6	ees . magaaggagaaaaa.	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
\dj. Flow (vph)	766	65	43	1022	87	60	
Shared Lane Traffic (%)							
ane Group Flow (vph)	831	0	43	1022	87	60	
urn Type			pm+pt			Prot	
Protected Phases	2		1	12	4	4	
Permitted Phases			12	2	4		
etector Phase	2		1	1 2	4	4	
Switch Phase							
/linimum Initial (s)	15.0		6.0		6.0	6.0	is de la constanción
vlinimum Split (s)	20.0		9.1		11.0	11.0	
Total Split (s)	42.0	0.0	8.0	50.0	10.0	10.0	AGUST V. T. SAMMER GENERAL MARINE MARINE MARINE PAR AND A MARINE
Total Split (%)	70.0%	0.0%	13.3%	83.3%	16.7%	16.7%	
Maximum Green (s)	37.0	0.070	4.9	00.070	5.0	5.0	
ellow Time (s)	3.0		3.0		3.0	3.0	
All-Red Time (s)	2.0		0.1		2.0	2.0	
ost Time Adjust (s)	0,0	0.0	0.0	0.0	0.0	0.0	
otal Lost Time (s)	5.0	4.0	3.1	3.1	5.0	5.0	
_ead/Lag	Lag		Lead				
ead-Lag Optimize?	Section beautiful to a section of the section of th	die Malaimania				- idalimid <u>- 1</u> 1	
/ehicle Extension (s)	3.0		2.0		2.0	2.0	
Recall Mode	C-Max	non in the states deposite	None	a, i sa ga	None	None	
act Effet Green (s)	38.8		45.8	49.5	5.0	5.0	BUTTON TO THE STATE OF THE STAT
ctuated g/C Ratio	0.65		0.76	0.82	0.08	0.08	
/c Ratio	0.70		0.10	0.66	0.59	0.32	
Control Delay	11.4		2.5	4.7	45.3	13.4	
Queue Delay	0.0		0.0	0.1	0.0	0.0	
otal Delay	11.4		2.5	4.8	45.3	13.4	
os	В		A	A	D	В	
Approach Delay	11.4			4.7	32.3		наминика, д. т. (140°), «друг», с исламення принципання принципання принципання (2000) до ставов.
Approach LOS	В			Å	C		
Queue Length 50th (ft)	175		3	137	31	0	

	→ `	¥			
Queue Length 95th (ft)	302	m3	m137	#87	30
Internal Link Dist (ft)	376		281	253	
Turn Bay Length (ft)		70			
Base Capacity (vph)	1195	432	1537	148	187
Starvation Cap Reductn	0	0	27	0	0
Spillback Cap Reductn	0	0	0	0	0
Storage Cap Reductn		0	0	0	0
Reduced v/c Ratio	0.70	0.10	0.68	0.59	0.32

Other

Cycle Length: 60

Actuated Cycle Length: 60

Offset: 0 (0%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 70

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.70

Intersection Signal Delay: 9.4

Intersection LOS: A

Intersection Capacity Utilization 62.0%

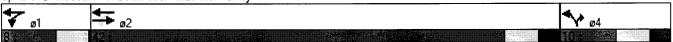
ICU Level of Service B

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

m Volume for 95th percentile queue is metered by upstream signal.



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		i				. '						32
Lane Configurations		4TÞ			44	7	74	î.		ሻ	†	7
Volume (vph)	125	805	85	20	855	230	345	130	15	200	55	220
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	11	. 11	13	11	11	16	11	13	13	11	11	13
Storage Length (ft)	0		125	0		25	230		0	300		300
Storage Lanes	0		1	0		1	1		0	1		1
Taper Length (ft)	25		25	25		25	25		25	25		25
Lane Util. Factor	0.95	0.95	0.95	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.987		i, washidadadiii		0.850		0.985	tegennofeloftafaata			0.850
FIt Protected		0.994			0.999		0.950			0.950		
Satd. Flow (prot)	0	3357	0	0	3418	1794	1711	1896	0	1711	1801	1636
Flt Permitted		0.591			0.907		0.511			0.657		
Satd. Flow (perm)	0	1996	0	0	3103	1794	920	1896	0	1183	1801	1636
Right Turn on Red		1330	Yes		0100	Yes	JEU		No:	1100	1001	No
Satd. Flow (RTOR)		15	103			, 66						
	n in a right or	30			30			30			30	
Link Speed (mph)					822			621			552	
Link Distance (ft)		209						14.1			12.5	
Travel Time (s)	0.00	4.8	0.00	0.00	18.7	^ ^^	0 00		V VV	A 00		Λ 02
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	136	875	92	22	929	250	375	141	16	217	60	239
Shared Lane Traffic (%)		1981181244		· . · · · · · · · · · · · · · · · · · ·								
Lane Group Flow (vph)	0	1103	0	_ 0	951	250	375	157	0	217	60	239
Turn Type	pm+pt			Perm		Prot	pm+pt	orana naba206.		pm+pt	pa - 1 1 <u>-</u>	pt+ov
Protected Phases	1	12		_	2	2	3	8		7	4	4 1
Permitted Phases	12			2	2		8	8		4	4	na arabanin ya y
Detector Phase	1	12		2	2	2	3	8		7	4	41
Switch Phase												
Minimum Initial (s)	6.0			15.0	15.0	15.0	6.0	6.0		6.0	6.0	
Minimum Split (s)	10.0			20.5	20.5	20.5	10.0	10.9		10.0	10.9	
Total Split (s)	13.0	54.0	0.0	41.0	41.0	41.0	21.0	20.0	0.0	16.0	15.0	28.0
Total Split (%)	14.4%	60.0%	0.0%	45.6%	45.6%	45.6%	23.3%	22.2%	0.0%	17.8%	16.7%	31.1%
Maximum Green (s)	9.0			35.5	35.5	35.5	17.0	15.1		12.0	10.1	
Yellow Time (s)	3.0			3.0	3.0	3.0	3.0	3.9		3.0	3.9	
All-Red Time (s)	1.0		i – jegtara Vilo	2.5	2.5	2.5	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	4.0	4.0	4.0	5.5	5.5	5,5	4.0	4.9	4.0	4.0	4.9	4.9
Lead/Lag	Lead			Lag	Lag	Lag	Lead	Lag		Lead	Lag	
Lead-Lag Optimize?				- 3								
Vehicle Extension (s)	0.2			0.2	0.2	0.2	2.0	2.0		2.0	2.0	
Recall Mode	Max			C-Max	C-Max	C-Max	None	None		None	None	
Act Effct Green (s)		46.7	Constituti (Bostonista) (B		35.5	35.5	31.3	15.4		21.8	9.9	23.6
Actuated g/C Ratio		0.52			0.39	0.39	0.35	0.17		0.24	0.11	0.26
v/c Ratio		0.93	and the second s	an Gorffakartii.	0.78	0.33	0.81	0.48		0.62	0.30	0.56
Control Delay		31.9			29.2	15.2	39.7	39.5		31.0	41,2	34.8
Queue Delay		0.0			0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay		31.9			29.2	15.2	39.7	39.5		31.0	41.2	34.8
LOS											41.2 D	
		C			C	В	D	D		С		
Approach Delay		31.9			26.3			39.6			33.9	
Approach LOS		С			С			D			С	

	→ → →	✓ ←	*	4	†	1	-	↓	4
Service of the servic								Ng.	ā şla
Queue Length 50th (ft)	201	243	69	173	82		90	32	118
Queue Length 95th (ft)	#337	321	127	#302	143		150	70	195
Internal Link Dist (ft)	129	742			541			472	
Turn Bay Length (ft)			25	230			300		3 00
Base Capacity (vph)	1189	1224	748	470	325		371	202	415
Starvation Cap Reductn	0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.93	0.78	0.33	0.80	0.48		0.58	0 .30	0.58

Area Type: Other

Cycle Length: 90

Actuated Cycle Length: 90

Offset: 46 (51%), Referenced to phase 2:EBWB, Start of Yellow

Natural Cycle: 65

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.93

Intersection Signal Delay: 31.4

Intersection LOS: C
ICU Level of Service F

Intersection Capacity Utilization 92.3%

Analysis Period (min) 15

Splits and Phases: 11: Bank St & Franklin St



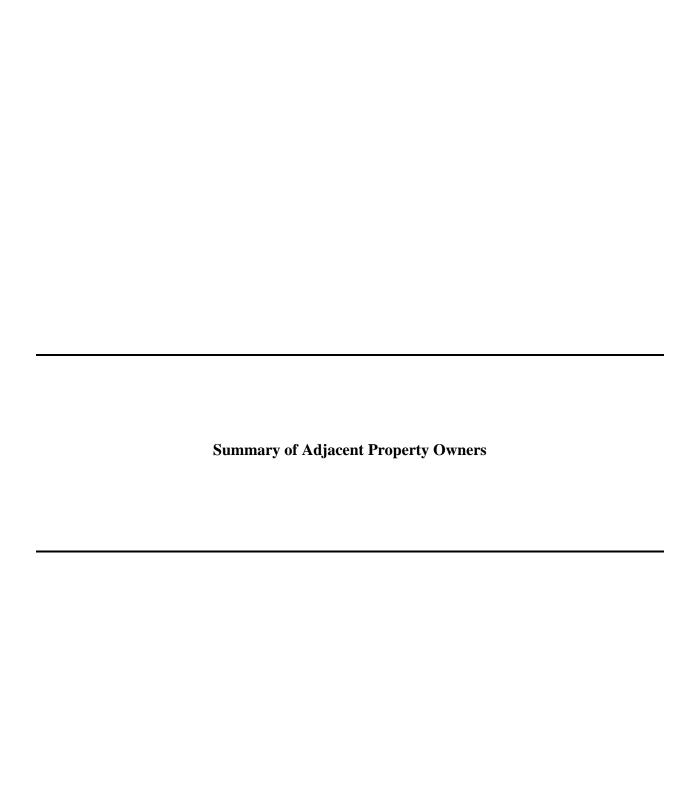
^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

	→	•	6	4	4	<i>></i>				
	-	7	•		1					
Lane Configurations	f)			€Î	¥					
Volume (veh/h)	725	40	160	990	0	165				
Sign Control	Free			Free	Stop					u an annumura energen vilin ni mina
Grade	0%			0%	0%					
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92		annan i tog minima		. regionalismosti i dell'ille cole
Hourly flow rate (vph)	788	43	174	1076	0	179				
Pedestrians Lane Width (ft)				Power 1 high						
Walking Speed (ft/s)	F-1			átologi. T						
Percent Blockage										
Right turn flare (veh)										
Median type	None			None						5,
Median storage veh)		e e e e e e e e e e e e e e e e e e e			i aran werdi		Ter - 111; 12: 1111111111111111			**************************************
Upstream signal (ft)	361			275						
pX, platoon unblocked			0.67		0.52	0.67				
vC, conflicting volume			832		2234	810				
vC1, stage 1 conf vol										
vC2, stage 2 conf vol					r					Fig. 1
vCu, unblocked vol		r skilannen salkgregt	500	SPERIOR BURBURACO ()	1477	468				
tC, single (s)			4.1		6.4	6.2				
tC, 2 stage (s) tF (s)			2.2		3.5	3.3				
p0 queue free %			76		100	5.5 55				BIV WINDSOLDER FO
cM capacity (veh/h)			711		55	398				
							va 1906 lietus tuttelli			
Volume Total	832	1250	179							
Volume Left	0	174	0				rper neatest nechilin			
Volume Right	43	0	179							
cSH	1700	711	398							
Volume to Capacity	0.49	0.24	0.45							
Queue Length 95th (ft)	0	24	57							
Control Delay (s)	0.0	8.3	21.3							
Lane LOS	. His in a shipping and the second	Α	С	Telephonologica surfici		not popoleta natalia i si se				ын он этринескийн с. ин 16 с
Approach Delay (s) Approach LOS	0.0	8.3	21.3 C							
Associate and a second										
Average Delay			6.3							
Intersection Capacity Utiliza	ation		121.7%	IC	U Level o	f Service			4	
Analysis Period (min)			15							

	-	•	•	←	4	<i>F</i>	
Lane Configurations	ĵ >		*		ሻ	7	
Volume (veh/h)	910	40	155	1125	20		
Sign Control	Free			Free	Stop		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph) Pedestrians	989	43	168	1223	22	98	
Lane Width (ft) Walking Speed (ft/s)							
Percent Blockage Right turn flare (veh)							
Median type	None			None			
Median storage veh)	ilia in individuali	enthireas de viletta e	n en i i i jo Tijo tipati	· · · · · · · · · · · · · · · · · · ·			
Jpstream signal (ft)	175			1318			
X, platoon unblocked			0.66		0.72	0.66	
/C, conflicting volume			1033		2571	1011	
C1, stage 1 conf vol					and an arrangement of the second		
/C2, stage 2 conf vol						1.00	
/Cu, unblocked vol			796		1935	763	
C, single (s)			4,1		6.4	6.2	
C, 2 stage (s)			2.2		3.5	3.3	
tF (s) p0 queue free %			2.2 69		3.5 40	64	-ratif
cM capacity (veh/h)			548		36	268	
	se, takai illi					en in de Ma che (1942) (2005) and State (1945) and the contract of the contra	
Volume Total	1033	168	1223	22	98		
Volume Left	0	168	0	22	0		
/olume Right	43	0	0	0	98	1.00	
SH	1700	548	1700	36	268		
/olume to Capacity	0.61	0.31	0.72	0.60	0.36		
Queue Length 95th (ft)	0	32	0	52	40	internation of the control of the co	
Control Delay (s) Lane LOS	0,0	14.5	0.0	201.7	25.9		
Approach Delay (s) Approach LOS	0.0	B 1.8		F 57.9 F	D		
.581-							
Average Delay			3.7				
Intersection Capacity Utiliza	ation		72.2%	i ic	U Level o	of Service C	
Analysis Period (min)	america care a mercilian		15		es a mortum Millid	annan marka 12 milyon ya eserika kerindan kanan manan manan manan manan manan menye esimber ya kerinda kerinda	

	→	_	←	*	\	4	
S1							
Lane Configurations	×	*	(أ				
Volume (veh/h)	5	1000	1280	95	0	0	
Sign Control		Free	Free		Stop		HT HTT I THE STREET
Grade		0%	0%		0%	The state of the s	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	5	1087	1391	103	0	0	
Pedestrians			entra contrata de la				
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (ft)		612	881				
pX, platoon unblocked	0.49				0.68	0.49	
vC, conflicting volume	1495				2541	1443	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1489				1749	1384	m secret constraines. L.S.ded
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)			s a second constant to the			ver n. 4. 2 m., n. n. c. spolice de la company de la compa	acosas propieros N. P. el 1878
tF (s)	2.2				3.5	3.3	
p0 queue free %	98			annin dedaggi ga sah	100	100	
cM capacity (veh/h)	221				63	86	
Volume Total	5	1087	1495			72	
Volume Left	5	0	1433				
Volume Right	0	0	103				
cSH	221	1700	1700				
Volume to Capacity	0.02	0.64	0.88				
Queue Length 95th (ft)	2	0.07	0.00				
Control Delay (s)	21.7	0.0	0.0				lab Papagaga
Lane LOS	C	0.0	. YIY	Pakit tit et et		tadilida par te priyesas 1.29 diyeridi birili di bili di	
Approach Delay (s)	0.1		0.0				waida is it.
Approach LOS			· · · · · · · · · · · · · · · · · · ·			mannene – 92 – 5 – Kalvi saksisaisiainin merekaksiksi ilili ilistessä tivi	e Waster of State and Comment
Bico.							
Average Delay			0.0				
Intersection Capacity Utiliza	ition		76.5%	IC	:U Level	f Service D	
Analysis Period (min)			15				





Property Owner (N/F) Location **Bank Street** #80 PASJ, LLC Dongs Realty of Seymour, LLC #82-84 #98 Town of Seymour Trust Realty Corp. #100 #79-101 Doris M. Tkacz Living Trust Richard Sobotka #111-113 #115 Elaine Larsen Fatima C. Silva #117-119 Ronald E. & Lucretia M. Kurtz #123-125 #127 Leonard Remetta, Sr. #144 Lots 70A&70B Associates, LLC #145 MJBANK, LLC #200 State of Connecticut (Fisheries) #225 RAB I, LLC #235 McDonald's Corporation #240 Stanley G. Ostaszeski #246 Swan Avenue Associates, LLC TD BankNorth, N.A. #249 #252 NAMO, LLC #253-255 Paul Filipowich (III), et al Seymour-Oxford Nursery & Child #256 Carl J. (III) & Patricia K. Miller #260 #277 Klarides Family Associates, LLC **Beecher Street** #23-24 Gina Affinito #25 Joseph Cavanaugh **Church Street** Russian American Citizens Club #20 #22 Ronald J. Fredericks **Franklin Street** #7-9 Dongs Realty of Seymour, LLC #10 Town of Seymour **Johnson Avenue** Stanley M. Meholik, Jr., et al #10 Martha Street

Robert E. Simpson

Guy E. & Gale E. Greco

Housatonic Wire Company

#7

#20

#109

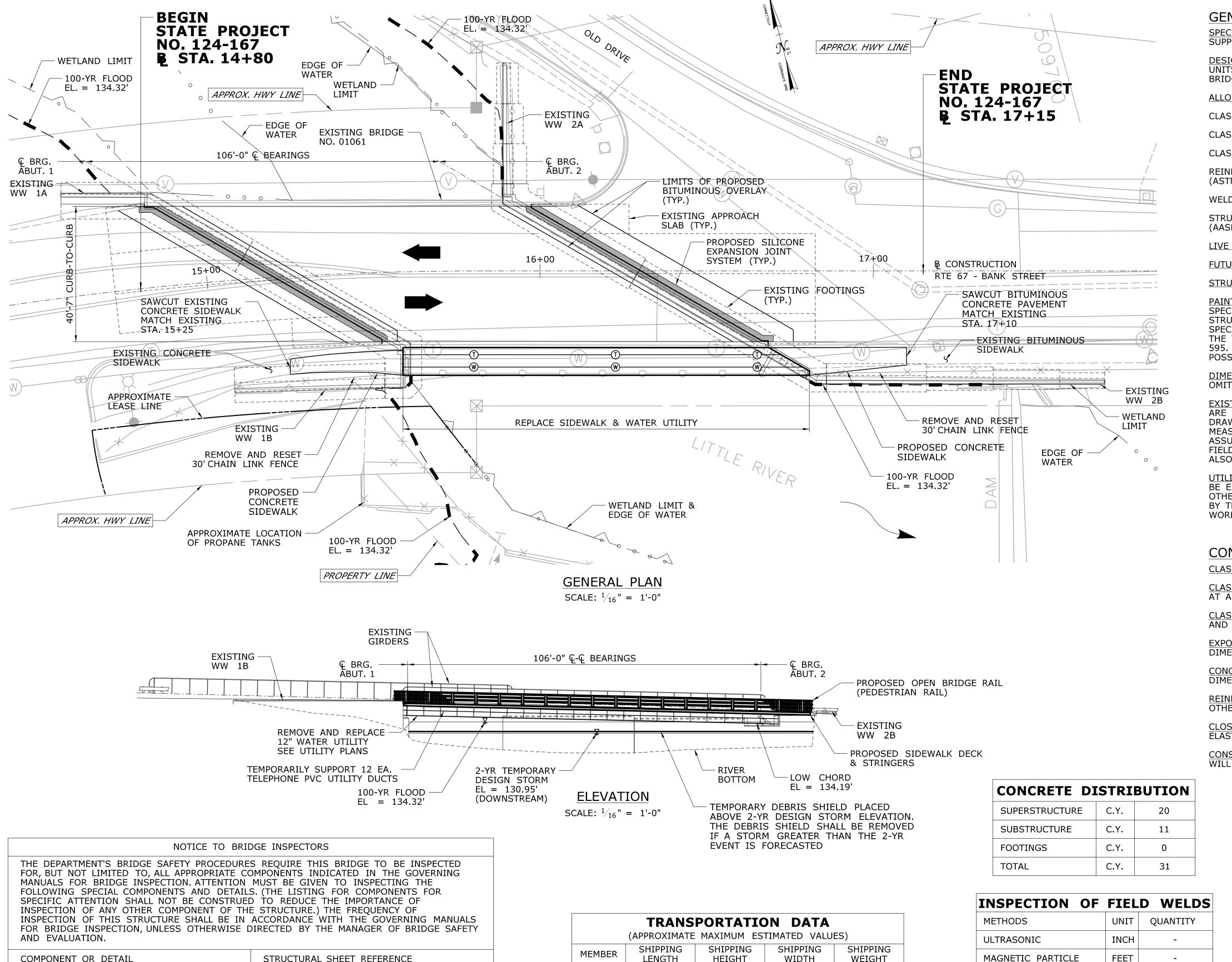
Old Drive

River Street

MILONE & MACBROOM®







GENERAL NOTES

SPECIFICATIONS: CONNECTICUT DEPARTMENT OF TRANSPORTATION FORM 816 (2004), SUPPLEMENTAL SPECIFICATION DATED JANUARY 2013 AND SPECIAL PROVISIONS.

DESIGN SPECIFICATIONS: AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, CUSTOMARY UNITS 2012, AS SUPPLEMENTED BY THE CONNECTICUT DEPARTMENT OF TRANSPORTATION BRIDGE DESIGN MANUAL (2003).

ALLOWABLE DESIGN STRESSES:

... BASED ON f'c = 3,000 psiCLASS 'A' CONCRETE.... CLASS 'C' CONCRETE..... BASED ON f'c = 3,000 psi

CLASS 'F' CONCRETE..... BASED ON f'c = 4,000 psi

REINFORCEMENT

(ASTM A615 GRADE 60)...... Fy = 60,000 psi

WELDED WIRE FABRIC (ASTM A185).....Fy = 75,000 psi

STRUCTURAL STEEL

(AASHTO M270, GRADE 50)......Fy = 50,000 psi

LIVE LOAD: AASHTO HL-93

FUTURE PAVING ALLOWANCE: NONE

STRUCTURAL STEEL: SEE STRUCTURAL STEEL NOTES FOR DESIGNATIONS AND REQUIREMENTS.

PAINT: PAINT FOR EXISTING STEEL SHALL CONFORM TO THE REQUIREMENTS OF THE SPECIAL PROVISION FOR THE ITEM "ABRASIVE BLAST CLEANING AND FIELD PAINTING OF STRUCTURE." PAINT FOR NEW STEEL SHALL CONFORM TO THE REQUIREMENTS OF THE SPECIAL PROVISION FOR THE ITEM "STRUCTURAL STEEL - MISCELLANEOUS." THE COLOR OF THE TOPCOAT MATERIAL ON THE STRUCTURAL STEEL SHALL CONFORM TO FEDERAL STANDARD 595. FINAL PAINT COLOR OF THE TOP COAT TO MATCH EXISTING AS CLOSELY AS POSSIBLE.

<u>DIMENSIONS</u>: WHEN DIMENSIONS ARE GIVEN TO LESS THAN THREE DECIMAL PLACES, THE OMITTED DIGITS SHALL BE ASSUMED TO BE ZEROS.

EXISTING DIMENSIONS: DIMENSIONS OF THE EXISTING STRUCTURE SHOWN ON THESE PLANS ARE FOR GENERAL REFERENCE ONLY. THEY HAVE BEEN TAKEN FROM THE ORIGINAL DESIGN DRAWINGS AND ARE NOT GUARANTEED. THE CONTRACTOR SHALL TAKE ALL FIELD MEASUREMENTS NECESSARY TO ASSURE PROPER FIT OF THE FINISHED WORK AND SHALL ASSUME FULL RESPONSIBILITY FOR THEIR ACCURACY, WHEN SHOP DRAWINGS BASED ON FIELD MEASUREMENTS ARE SUBMITTED FOR APPROVAL, THE FIELD MEASUREMENTS SHALL ALSO BE SUBMITTED FOR THE REFERENCE BY THE REVIEWER.

<u>UTILITIES</u>: THE LOCATION OF EXISTING UNDERGROUND UTILITIES ARE NOT WARRANTED TO BE EXACT, NOR IS IT WARRANTED THAT ALL UNDERGROUND PIPES, CABLES, CONDUITS, OR OTHER UTILITIES ARE SHOWN. THE ACTUAL LOCATION OF UTILITIES SHALL BE DETERMINED BY THE CONTRACTOR, ALL UTILITY COMPANIES SHALL BE NOTIFIED 30 DAYS PRIOR TO ANY WORK AFFECTING PIPES, CABLES, OR UTILITIES,

CONCRETE NOTES

FEET

INCH

44

RADIOGRAPHIC

CLASS 'A' CONCRETE: CLASS 'A' CONCRETE SHALL BE USED FOR ABUTMENT BACKWALLS.

CLASS 'C' CONCRETE: CLASS 'C' CONCRETE SHALL BE USED FOR CONCRETE SIDEWALK AT APPROACHES TO BRIDGE. (HIGHWAY ITEM)

CLASS 'F' CONCRETE: CLASS 'F' CONCRETE SHALL BE USED FOR SIDEWALK DECK ON BRIDGE AND REBUILT PORTIONS OF APPROACH SLABS AND BRIDGE DECK.

EXPOSED EDGES: EXPOSED EDGES OF CONCRETE SHALL BE BEVELED 1"x1" UNLESS DIMENSIONED OTHERWISE.

CONCRETE COVER: ALL REINFORCEMENT SHALL HAVE TWO INCHES COVER UNLESS DIMENSIONED OTHERWISE.

REINFORCEMENT; ALL REINFORCEMENT SHALL BE ASTM A615 GRADE 60 UNLESS NOTED OTHERWISE.

CLOSED CELL ELASTOMER: THE COST OF FURNISHING AND INSTALLING CLOSED CELL ELASTOMER SHALL BE INCLUDED IN THE COST OF THE ITEM "CLASS 'F' CONCRETE."

CONSTRUCTION JOINTS: CONSTRUCTION JOINTS, OTHER THAN THOSE SHOWN ON THE PLANS, WILL NOT BE PERMITTED WITHOUT THE PRIOR APPROVAL OF THE ENGINEER.

HYDRAULIC DATA	
DRAINAGE AREA (SQ. MI.)	15.5
DESIGN FREQUENCEY (YR)	100
DESIGN DISCHARGE (CFS)	2270
AVG. DAILY FLOW ELEV. (FT) OBSERVED JUNE, 2009	128.5
UPSTREAM DESIGN WATER SURFACE ELEV. (FT)	135.38
DOWNSTREAM DESIGN WATER SURFACE ELEV. (FT)	134.32
MAXIMUM SCOUR ELEVATION (FT)	ON ROCK

DRAWING TITLE

SEYMOUR

GENERAL PLAN &

ELEVATION

124-167

S-02

03.02

HEET NO.

		DESIGNER/DRAFTER:	A \$803 A	SIGNATURE/	PROJECT TITLE:
	THE INFORMATION, INCLUDING ESTIMATED QUANTITIES OF WORK, SHOWN ON THESE SHEETS IS BASED ON LIMITED INVESTIGATIONS BY THE STATE AND IS IN NO WAY WARRANTED TO INDICATE THE CONDITIONS OF ACTUAL QUANTITIES	DEH CHECKED BY: RRC	STATE OF CONNECTICUT DEPARTMENT OF TRANSPORTATION	CME ASSOCIATES, INC. 333 East River Drive. Suite 400	REHABILITATION OF BRIDGE NO. 01061
	OF WORK WHICH WILL BE REQUIRED.	SCALE AS NOTED	DEFARIMENT OF TRANSPORTATION	East Hartford, CT 06108	ROUTE 67 OVER LITTLE RIVER

HEIGHT

WIDTH

0'-8"

WEIGHT

1,900 lbs

LENGTH

Filename: ...\SB_Br01061_S_02_GenPlan.dgn

SIDEWALK

STRINGER

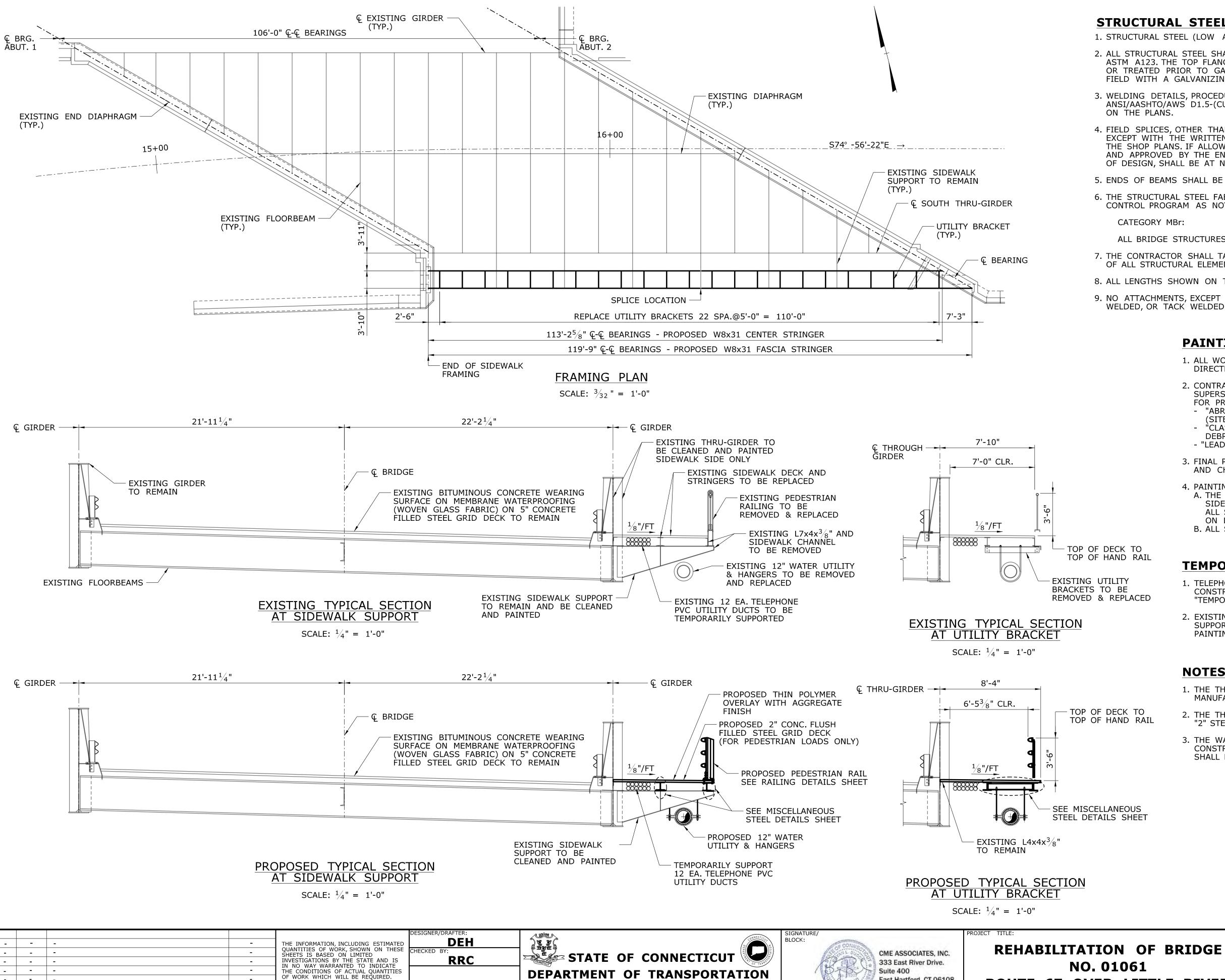
STRUCTURAL SHEET REFERENCE

SHEET NO. Plotted Date: 9/9/2013

COMPONENT OR DETAIL

REVISION DESCRIPTION

REV. DATE



Filename: ...\SB_Br01061_S_04_Framing.dgn

SCALE AS NOTED

- | - | -

REV. DATE

REVISION DESCRIPTION

SHEET NO. Plotted Date: 9/9/2013

STRUCTURAL STEEL NOTES:

- 1. STRUCTURAL STEEL (LOW ALLOY) SHALL CONFORM TO AASHTO M270, GRADE 50 T2.
- 2. ALL STRUCTURAL STEEL SHALL BE HOT-DIP GALVANIZED IN ACCORDANCE WITH ASTM A123. THE TOP FLANGE OF STRINGERS AND SPLICE LOCATIONS SHALL BE MASKED OR TREATED PRIOR TO GALVANIZING. SPLICE LOCATIONS SHALL BE TOUCHED UP IN THE FIELD WITH A GALVANIZING COMPOUND IN ACCORDANCE WITH THE SPECIAL PROVISIONS.
- 3. WELDING DETAILS, PROCEDURES, AND TESTING METHODS SHALL CONFORM TO THE ANSI/AASHTO/AWS D1.5-(CURRENT) - BRIDGE WELDING CODE, UNLESS OTHERWISE NOTED
- 4. FIELD SPLICES, OTHER THAN THOSE SHOWN ON THE PLANS, WILL NOT BE ALLOWED EXCEPT WITH THE WRITTEN PERMISSION OF THE ENGINEER PRIOR TO THE SUBMISSION OF THE SHOP PLANS. IF ALLOWED, THESE SPLICES SHALL BE DESIGNED BY THE CONTRACTOR AND APPROVED BY THE ENGINEER. THE COST OF THESE SPLICES, INCLUDING THE COST OF DESIGN, SHALL BE AT NO ADDITIONAL EXPENSE TO THE STATE.
- 5. ENDS OF BEAMS SHALL BE VERTICAL AFTER THE APPLICATION OF FULL DEAD LOADS.
- 6. THE STRUCTURAL STEEL FABRICATORS SHALL BE CERTIFIED UNDER THE AISC QUALITY CONTROL PROGRAM AS NOTED BELOW:

ALL BRIDGE STRUCTURES OTHER THAN UNSPLICED ROLLED BEAM BRIDGES.

- 7. THE CONTRACTOR SHALL TAKE THE PROPER PRECAUTIONS TO ENSURE THE STABILITY OF ALL STRUCTURAL ELEMENTS UNTIL THE TOTAL STRUCTURE IS IN BEING.
- 8. ALL LENGTHS SHOWN ON THE PLANS ARE HORIZONTAL.
- 9. NO ATTACHMENTS, EXCEPT AS SHOWN ON THE PLANS, SHALL BE FILLET WELDED, PLUG WELDED, OR TACK WELDED TO THE BOTTOM FLANGES

PAINTING NOTES:

- 1. ALL WORK SHOWN ON THIS DRAWING SHALL BE PERFORMED WHERE DIRECTED BY THE ENGINEER.
- 2. CONTRACTOR'S ATTENTION IS CALLED TO THE FACT THAT EXISTING SUPERSTRUCTURE PAINT MAY CONTAIN LEAD. SEE SPECIAL PROVISIONS FOR PROCEDURES AND SUBMITTALS OF:
- "ABRASIVE BLAST CLEANING AND FIELD PAINTING OF STRUCTURES (SITE NO. 1)"
- "CLASS 1 CONTAINMENT AND COLLECTION OF SURFACE PREPARATION
- DEBRIS" - "LEAD HEALTH PROTECTION PROGRAM (LHPP)"
- 3. FINAL PAINT COLOR SHALL CONFORM TO FEDERAL STANDARD 595, AND CHOSEN TO MATCH EXISTING PAINT AS CLOSELY AS POSSIBLE.
- 4. PAINTING LIMITS ARE AS FOLLOWS:
- A. THE SOUTH SIDE OF THE SOUTH THRU-GIRDER FROM THE TOP OF SIDEWALK CANTILEVER SUPPORTS TO THE TOP FLANGE, INCLUDING ALL STIFFENERS. SEE "TYPICAL SIDEWALK AT FLOORBEAM" SECTION ON DRAWING NO. S-07
- B. ALL SURFACES OF SIDEWALK CANTILEVER SUPPORTS.

TEMPORARY SUPPORT OF UTILITIES:

- 1. TELEPHONE CONDUITS SHALL BE TEMPORARILY SUPPORTED DURING CONSTRUCTION. THIS WORK SHALL BE PAID FOR UNDER THE ITEM "TEMPORARY SUPPORT OF UTILITIES,"
- 2. EXISTING SIDEWALK SUPPORTS MAY BE USED TO TEMPORARILY SUPPORT UTILITIES BUT ADEQUATE SPACE TO FACILITATE CLEANING, PAINTING, AND RECONSTRUCTION OF THE SIDEWALK IS REQUIRED.

NOTES:

ROUTE 67 OVER LITTLE RIVER

East Hartford, CT 06108

- 1. THE THIN POLYMER OVERLAY SHALL BE APPLIED IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS.
- 2. THE THIN POLYMER OVERLAY SHALL BE PAID FOR UNDER THE ITEM "2" STEEL GRID FOR BRIDGE SIDEWALK".
- 3. THE WATER UTLITY SHALL BE REMOVED FOR THE DURATION OF CONSTRUCTION. BYPASS AND RECONSTRUCTION OF WATER UTILITY SHALL BE IN ACCORDANCE WITH UTILITY PLANS.

SEYMOUR

FRAMING PLAN &

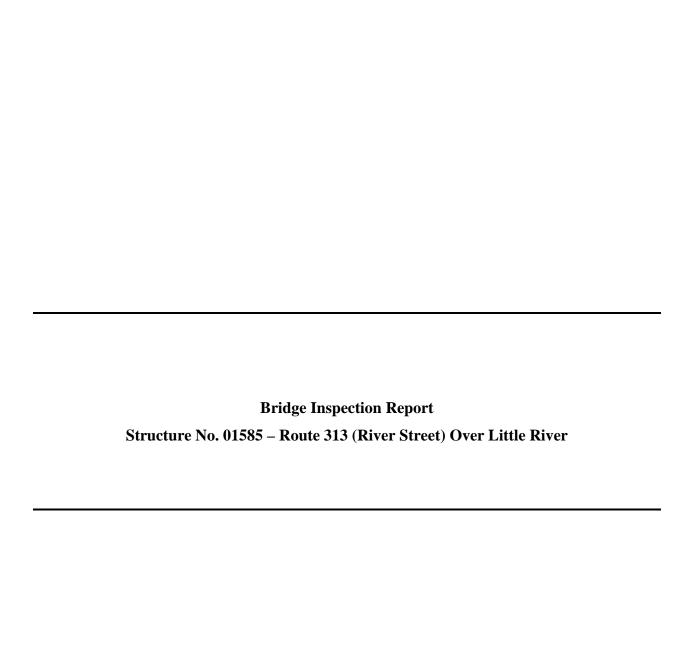
TYPICAL SECTIONS

124-167

S-04

03.04

HEET NO.





Structure No. 0 1585

Route 313 (River Street)

over

Little River

Seymour

Mile Point 0.04

Routine Inspection on 15-Nov-11

Inspected By Team No. 8 - CTDOT - Bridge Safety

For Area No. 5

TEAM:	Forwarded to T.E. 3. D. PAWLIKOWSK	, !	Date: /2 /3 /7
TE. 3:	Reviewed By T.E. 3: D PAW 41/10 ws/1.		Date. 12 14 11
	BMM Required	20	
	Town Structure	20	
	Rating <= 5 {Item Nos. 58, 59, 60, 61 or 62}	10	
	Forwarded to Supervisor		Date:
	Forwarded to "To Be Copied Drawer"		Date /3 /9//
	Date BRI-19 Entered 10 1411		
SUPER	VISOR: Reviewed By Supervisor		Date
Support	Date Copies Made:	BMM No.	
	Scanned By Date:		PDF Box No.:

NBIS: Yes

Last Inspection Date: November 10, 2009

State of Connecticut - Department of Transportation Bureau of Engineering & Construction - Bridge Safety & Evaluation

Bridge No: 0 1585 Town: Seymour

Location: Route 313 (River Street) over Little River

Inspection Date: November 15, 2011

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Abutment Stem Work Sheet

Bridge No.: 0 1585 Town: Seymour

Facility Carried\Feature Intersected: Route 313 {River Street} over Little River

Abutment Stem No. or Nos.: Abutment Nos. 1 & 2

Abutment Stem Design Type: Full Height\Closed Abutments - Cantilever

Abutment Stem Material Type: Concrete

Abutment Stem Foundation Type: Spread Footings Founded on Rock

Item No. 113 Scour Critical: - 8 -

Tidal: No Rip Rap: Yes

Exposed Footing: No

Footing Undermining: No

Sheet Piles - Timber or Steel: No

Bed Rock: No Concrete Apron: No

Abutment Stem - In Water - At Normal Stage:

Normal Stage - The water stage prevailing during the greater part of the year.

Comments: Bridge Plans - Project No. 124 - 11 - Year 1936

Abutment No. 1 Footing Height - 3 feet 8 inches & 4 feet 5 inches - per plans

Abutment No. 1 Footing Width - 13 feet 6 inches & 15 feet 00 inch - per plans

Abutment No. 2 Footing Height - 3 feet 6 inches - per plans

Abutment No. 2 Footing Width - 12 feet 00 inch - per plans

Wingwall Footing Height - Varies 3 feet 6 inches to 5 feet 00 inch - per plans

Wingwall Footing Width - Varies 9 feet 00 inch to 15 feet 00 inch - per plans

Prepared By: David Pawlikowski, P.E.

CTDOT - Bridge Safety

Date: December 14, 2011

Connecticut Department of Transportation

Bridge Inspection Report BRI-18

Bridge #: 01585				Inspe	ection Date: 11/15/2011
nspection Type:	-	utine	Previous Inspection	11/10/2009	Snooper No Required:
nspection Perform	ed Te	am 8	Feature Carried:	ROUTE 31	Snooper Used: No
Town:	SE	YMOUR	Feature Intersected	: LITTLE RIVER	Year Built: 1936
Location:	21	1 FT E OF ROUT	Main Design:	Tee Beam	Year Rebuilt:
Main Material:	Co	ncrete]		
	Гетр:	Start Time:	End Time:	Inspectors:	Task:
11/15/2011	66	1:50:00 PM	3:20:00 PM	A. Ferrara	Lead Inspector
DECK:	Rati	Bitu tran	uminous concrete with wat nsverse cracking with mind	or areas of segre	
DECK-S'		12411 Inte	egral deck rating format. Pour y on the condition of the w	er CT. Bridge Ins earing surface.	spection Manual. Rating base
CURI	BS: 7.	No 14'	ncrete shows abrasion we rtheast approach curb exh 'potentail spall near deck e rb reveals at mid-span eas	ibits one vertical end.	crack open 3/16"+/- with a
MEDIA	AN: N	-			
SIDEWAL	KS: 7	Ne So	wer concrete sidewalk on uth end approach side wa	the east side. Ik has settled up	to 7/8"+/- at deck end.
PARAP	ET: 7	cra	st side has concrete parapacks extending across top eling.	pet with double a with some efflore	luminum railing.Vertical hairline escence and areas of rub coat
RAILI	NG: 6	llha	iginal concrete balustrade irline cracks at random loc d a 3/16"open diagonal cra	ations and a larg	exhibits light abrasion and ge surface spall 17"x 9"x 3"deep yest end post.

		Double aluminum rail on east side only; no note worthy defects.
PAINT:	N	-
FENCE:	N	-
DRAINS:	N	-
LIGHTING STANDARD:		
UTILITIES TYPE/SIZE:		8" Water main between beams-1 & 2 and is not seated in north hanger section. 24" Sewer pipe along the west side.
		2" gas pipe along the west side.
CONSTR JOINTS:	N	-
EXPANSION JOINTS:		Asphaltic plug joint seals exhibits areas of slightly exposed aggregate.

59. SUPERSTRUCTURI		Tee-Beam Overall 6
	Rating	
BEARING DEVICES:	6 ·	Limited view to front of plates. Abutment-1 bearings generally exhibits minor light to heavy rust. Abutment- 2 bearings are turning blue in color from reaction of different metals in plates.
STRINGERS:	N	-
GIRDERS:	6 ·	Concrete "T" Beams. Generally all beam webs exhibits numerous partial and full height hairline vertical cracks that continue from transverse cracks across the bottom of the beams.
		There are some beams the exhibits shallow spalls with exposed rebars at random locations on the vertical faces and some honeycomb areas and small potential spalls on the bottom faces.
		General note: Two newer T-Beams and abutment seats where added in the past to the east end.
FLOOR BEAMS:	N	-
TRUSSES- GENERAL:		
TRUSSES- PORTALS:		-
TRUSSES- BRACING:		
PAINT:		-
RUST:		See above.
MACHINERY MOV SPAN:		
RIVETS & BOLTS:	N	-
WELDS - CRACKS:	N	-
TIMBER DECAY:	N	-
CONCRETE CRACKING:	6 -	See above. The u-side of the deck exhibits approximately 2% of deterioration with transverse, longitudinal and a few diagonal hairline cracks. Noted were some map hairline cracks and a large surface spall with exposed rebar approximately 2-Sq ft.located in bay- 4 north end & one 8-Sq.ft. area of honeycombing at south end.
COLLISION DAMAGE:		
MEMBER ALIGNMENT:		
DEFLECT. UNDER	N	Normal.

LOAD:		1
VIBRATION UNDER LOAD:		Normal.
STAND PIPES:		
BARREL LADDERS:	N	-
		ARE BARREL LADDERS OSHA COMPLIANT? NA
60. SUBSTRUCTURE:	Concrete	Overall Rating: 7
SOBSTRUCTORE.	Rating	
ABUTMENTS- STEM:	7.	Abutments exhibits areas of light to medium abrasion and scaling along the base with hairline vertical cracks at random locations. The south abutment exhibits two slightly open vertical cracks under beams-3 & 5. The north abutment at west cheekwall exhibits a 1/8"+/- open crack with efflorescence approximately 3-ft.+/- long continuing into the cap. Newer section exhibits some hairline cracks with efflorescence.
ABUTMENTS- BACKWALL:	7.	Monolithic backwalls. Some minor hairline cracks at random locations. North end exhibits a patched spall over the sewer pipe.
ABUTMENTS- FOOTINGS:		Not visible.
ABUTMENTS- SETTLEMENT:		-
ABUTMENTS- WINGWALLS:		Wingwalls generally exhibits areas of minor abrasion and scaling with some minor hairline cracks and minor spalls. The northwest wingwall also exhibits an area of heavy-severe scaling located on top of wingwall approximately 9-ft.long x 10"wide.
PIERS/BENTS- CAPS:		
PIERS/BENTS-PILE BENT:		-
PIERS/BENTS- COLUMNS:		
PIERS/BENTS- FOOTING:		
PIERS/BENTS- SETTLMT:		
EROSION-SCOUR:		-
CONCRETE CRACK-SPALL:		See above.
STEEL CORROSION:		
PAINT:		
TIMBER DECAY:		

76.00	N	-
COLLISION DAMAGE:		-
DEBRIS:		-
61. CHANNEL & CHANNEL		Overall Rating:
PROTECTION:	Dating	
	Rating	
CHANNEL SCOUR:	6	Channel exhibits local scour along the northwest end due to poor channel alignment.
9 _ 1		Water depth up to 3-ft deep. See attached sheets.
EMBANKMENT EROSION:	8.	-
DEBRIS:	5	Obstruction - miscellaneous trash. Debris- shopping carts, tires.
VEGETATION:	5.	Heavy vegetation encroachment in the up stream channel.
CHANNEL CHANGE:	5 .	Stream bed aggradation and vegetation encroachment diverts low flow to the north side and into the northwest wingwall. General note Little River interfaces with Naugutuck River at the outlet end.
FENDER SYSTEM:	N	
SPUR, DIKES & JETTIES:		
RIP RAP:	8 .	Boulders.
62. CULVERTS & RETAINING WALL:	-	Overall Rating:
65. APPROACH	-	Overall Rating: 4
CONDITION	Rating	
APPROACH SLAB:	N	-
RELIEF JOINTS:	N	-
APPROACH GUIDE RAIL:	4 ·	Wood posts and cables at northwest end. Cables are loose and sagging on the ground. Unable to stop an erant vehicle.

		MBR on the east side. (8 rating).
APPROACH PAVEMENT:	7.	Bituminous Concrete exhibits areas of light segregation.
PAVEMENT.		South approach exhibits transverse, longitudinal and diagonal cracks.
		North approach exhibits transverse and longitudinal cracks with areas of ma type cracking in the southbound travel lane.
		There is 1-1/2" of settelment adjacent to the A.P.J on the north approach curblines.
APPROACH EMBANKMENT:	~ .	-

TRAFFIC SAFETY FEATURES

	Rating	
BRIDGE RAILINGS:	Last Inspection: 0 Current: 0	
TRANSITIONS:	Last Inspection: - 0 Current: 0	
APPROACH GUARDRAILS:	Last Inspection: 0 Current: 1	
APPR. GUARDRAIL ENDS:	Last Inspection: 0 Current: 1	

66. LOAD POSTING

	- Posted Loading -	
SINGLE UNIT (TONS):	Last Inspection: - Current: -	
SEMI TRAILER (TONS):	Last Inspection: - Current: -	
4 AXLE (TONS):	Last Inspection: - Current: -	
3S2 (TONS):	Last	-

	Inspection: -	II.	1
	Current: -		
ADVANCE WARNING (Y/N)		-	
LEGIBILITY		-	
VISIBILITY/LOCATION			
67. MISCELLANEOUS			
R	ating		
MIN. VERT. UNDERCLEARANCE:	Last Inspection:	-	
	Current: 20' 5"		
POSTED CLR.	Last Inspection:	•	
UNDER BRIDGE:	-' -" Current: -' -"		
POSTED CLR. ON	Last Inspection:	-	
BRIDGE:	_' _" Current: -' -"		
ADVANCED	The second secon	-	
WARNING (YES/NO):			
SPEED LIMIT (IF ANY):	Last Inspection:	pa .	
	Current: -		
CHARACTER OF TRAFIC:		(ADT) 5,500 - 4% Trucks.	
TION TO.			
ADDITIONAL NOTES:		Bridge ID's are in place.	
ADDITIONAL COMMENTS:		-	
COMMENTS:			
			12.17.11
Inspectors' Signatur	res: 1)	C. Formala	Date:
		1.	Date: 12,12,11
	2)	laha Plan	Date: 11/24/11
	7		
	3)		Date://

	4)	Date://
P.E. Signature:	m) /22	Date://
P.E. #:	३०९१ _५	Date: 12/14/11
Reviewed by:	_ond no conno	Date:

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Town:SEYMOURInspected by:JOHN CHAVEZFeature Carried:RT-31311/15/2011Feature Crossed:LITTLE RIVERProject No.:	SEYMOUR RT-313 Bate Inspected: LITTLE RIVER Project No.:	SEYMOUR RT-313 LITTLE RIVER Project No.:	Bridge No.	01585	Inspected by:	ANDREW FERRARA
RT-313 LITTLE RIVER Project No.:	RT-313 LITTLE RIVER Project No.:	RT-313 LITTLE RIVER Project No.:	Town:	SEYMOUR	Inspected by:	JOHN CHAVEZ
LITTLE RIVER	LITTLE RIVER	LITTLE RIVER	Feature Carried:	RT-313	Date Inspected:	11/15/2011
			Feature Crossed:	LITTLE RIVER	Project No.:	
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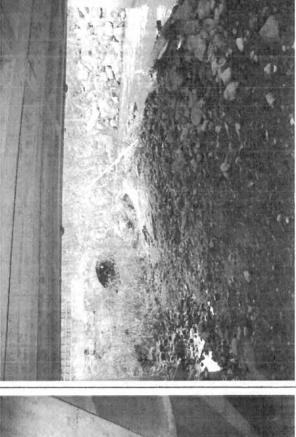


Photo # 15: View of Superstructure Underside.

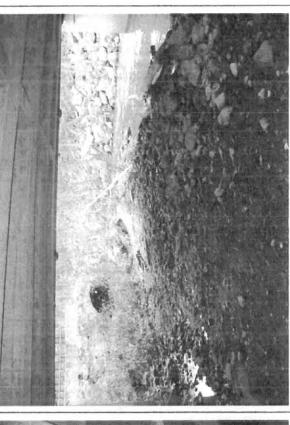


Photo # 16: View of Heavy Silt & Stone Buildup Under Structure.





公

Report of Meeting

DATE OF MEETINGS: October 13, 2015 –

Stakeholder Meeting No. 1

October 15, 2015 -

Stakeholder Meeting No. 2 October 19, 2015 – Public

Information Meeting

MMI #: 3211-02-4 STATE PROJECT NO.: 124-165

PROJECT: Route 67 (Bank Street)

Spot Improvements
Klarides Village to River

Street

Seymour, Connecticut

SUBJECT: Presentation of

Preliminary Engineering

Study

LOCATION: Norma Drummer Room –

Seymour Town Hall

1 First Street

Seymour, CT 06483

ATTENDEES:

Fred Messore, Director, Seymour Economic

Development

Mark Neilsen, Director of

Planning/Assistant Director, Naugatuck Valley Council of Governments (NVCOG) Rory Wilson, Administrative Assistant to

Seymour First Selectman

Anthony Ciriello, P.E., Principal, Director of Transportation – Milone & MacBroom, Inc.

(MMI)

Michael Joyce, P.E., Associate, Manager of

Highway Design – MMI Dilip Patel, P.E. – MMI Jennifer Martz – MMI

See attached list of attendees from the

public.

A public information meeting to discuss the Route 67 (Bank Street) Spot Improvements was held on October 19, 2015 to offer an opportunity for public comment and to discuss the information compiled and presented in the Preliminary Engineering Report dated February 19, 2014. Public Notice of the meeting was provided by the town in the *Republic American* on October 3, 2015. (See attached notice and verification from newspaper). In addition, prior to the formal public information meeting, the property owners immediately abutting the project limits were invited to attend two informal stakeholder workshops on October 13 and 15 at Town Hall to provide additional opportunities to receive information about the project, provide feedback, and gather information to support the public involvement process.

To begin the meeting, MMI representatives presented a general overview of the project and purpose of the preliminary engineering study and provided a more specific technical presentation of the project details as summarized below by using handouts provided to the public, existing photographs and photo simulations, colored renderings of the proposed design alternatives, and a computer-generated simulation showing the existing and future traffic conditions.



PROJECT LOCATION

The section of Route 67 (Bank Street) that falls within the study area (between River Street/Franklin Street and the westerly end of Klarides Village to the west) is approximately one-third of a mile. Bank Street generally runs in an east/west direction through the western part of town and provides connections to the town center area (via the Naugatuck River bridge) and to Oxford and points west. CT Route 8, which is elevated above the downtown area, provides regional access throughout the Naugatuck Valley region of Connecticut.

PROJECT PURPOSE

The purpose of this study is to evaluate and provide a palette of roadway and intersection enhancements along the CT Route 67 (Bank Street) corridor between River Street/Franklin Street and Klarides Village to the west in the town of Seymour, Connecticut.

This preliminary engineering study summarizes existing conditions, discusses the overall corridor issues and opportunities, outlines the right-of-way and regulatory permit implications, and summarizes the traffic and pedestrian network analyses conducted by MMI.

EXISTING CONDITIONS

Within the study area, Bank Street generally has a single travel lane in each direction with auxiliary turn lanes at various intersections. Sidewalks in various conditions are present along most of the project roadways, and the posted speed limit along Bank Street is 30 miles per hour (mph). The land uses through this corridor include retail, office, residential, and light industrial with the study area located within the C-2 General Commercial Zoning District, the CBD-1 Downtown Central Commercial District, and a small area of residential zoning (R-18) abutting Route 67 at the Beecher Street/Church Street intersection. The C-2 and CBD-1 districts define the limits of the Enterprise Corridor Zone.

Traffic Operations

The Connecticut Department of Transportation (CTDOT) records average daily traffic (ADT) volumes along state-owned highways. The ADT along Route 67, west of River Street and Franklin Street, was 20,000 vehicles per day (vpd) in 2009. The 85th percentile speeds along Bank Street are 36 mph for eastbound travel and 38 mph for westbound travel.

A traffic analysis was performed along Route 67 (Bank Street) at the following six intersections:

- Bank Street @ Franklin Street/River Street (CT Route 313)
- Bank Street @ Old Drive (east)
- Bank Street @ Church Street/Beecher Street
- Bank Street @ Old Drive (west)
- Bank Street @ Klarides Village Driveway/Johnson Avenue (unsignalized)
- Bank Street @ Klarides Village (signalized)

The peak hours for the corridor are 8:00 a.m. to 9:00 a.m. and 5:00 p.m. to 6:00 p.m. Bank Street carries between 1,070 and 1,350 vehicles during the morning peak hour depending on



the specific location. During the afternoon peak hour, 1,470 to 2,030 vehicles were counted. The analysis found that a greater percentage and overall number of heavy vehicles are present during the morning peak hour (1.5%) as opposed to the afternoon (.4%).

Accident Patterns

Using CTDOT accident records from January 2006 through December 2008, an analysis of the accident history along the corridor indicated there were 79 observed crashes. Of these, 63 resulted in property damage only while 16 resulted in personal injury. The crashes resulted from a variety of collision types: rear-end, fixed object, sideswipe, intersecting turns, and same-direction turns. The most prevalent crash type was rear-end, which is typical for signalized intersections.

Parking

On-street parking exists through the downtown area including areas along Bank Street that serve the adjacent retail establishments. Within the study limits, two on-street parking spaces are currently provided on the north side of Bank Street (near Franklin Street). On the south side of Bank Street, a wide shoulder supports "10-minute" on-street parking in front of several properties that are immediately adjacent to the Little River and currently have no on-site parking. The remaining parking areas along the corridor are provided within off-street parking facilities.

Regulatory Areas

The Route 67 (Bank Street) project corridor is located immediately west of the Naugatuck River. At two locations within the study area, the Little River is conveyed under the areas where improvements are proposed along Bank Street and under River Street (CT Route 313) to its confluence with the Naugatuck River. The Little River was studied in detail by the Federal Emergency Management Agency (FEMA), and specific floodplain elevations and floodway boundaries have been established.

In addition to the FEMA regulatory boundaries, field identification and delineation of Connecticut inland wetlands and federal wetlands within the project limits were performed. The wetland limits closely follow the floodplain boundaries and steep banks associated with the rivers. Regulated activities associated with the wetlands, watercourses, and the related upland areas may require local, state, or federal permit approvals.

Historic and Archaeological Significance

Within the project limits, there is one property that is eligible for the Register of National Historic Places. The design and construction of the improvements outlined within this report may need to be conducted in accordance with Section 106 under the National Historic Preservation Act.



Rights-of-Way Activities

Rights-of-way impacts to private property owners are discussed in more detail below and under various portions of the Preliminary Engineering Report.

PROPOSED IMPROVEMENTS

The following three improvement locations, as more specifically shown and described in the Preliminary Engineering Report dated February 2014, are highlighted as critical enhancement areas along with some operational improvements at two signalized intersections:

- Bank Street @ Franklin Street/River Street and @ Old Drive
- Bank Street @ Beecher Street/Church Street
- Bank Street @ Klarides Village/Johnson Avenue

Bank Street From Old Drive to Franklin Street/River Street (SR 313)

The preferred design for this section of Route 67 includes widening (primarily) on the south side of Bank Street between Old Drive East and the Franklin Street/River Street intersection. The concepts include the use of 11-foot lanes with 5-foot shoulders to support on-street bicycle connectivity from the areas adjacent to Bank Street to downtown Seymour and the developing riverfront recreational opportunities. The new edge of pavement and sidewalk create direct impacts to the buildings along the southern side of Bank Street including but not limited to direct impacts to the buildings and porches and the elimination of the limited "10-minute" on-street parking. In addition to the direct building impacts, the loss of parking constitutes a serious impact given the lack of on-site parking spaces and the current short-term on-street parking used by these properties and businesses. Full acquisition of these properties is likely and, therefore, is assumed in the cost analysis.

The preferred alternate also extends the westbound right-turn lane at the Walgreens driveway through to the intersection of Old Drive East to accommodate the traffic volumes at this location and continue the intended pedestrian and on-street bicycle patterns through the corridor.

Furthermore, the curb radius for the River Street right-turn lane northbound movement at the southeast corner of the intersection may be reduced substantially. The existing radius exceeds 150 feet, which is more than adequate for trucks making right turns northbound onto Bank Street. A reduced radius would serve to slow vehicles making this turn, shorten the distance for pedestrian crossings, and provide additional landscape area and possible connections to the town's Naugatuck River recreational resources.

Modifying the signal timing to provide additional green time for the Bank Street east/west phase will also be needed to improve the LOS at this intersection.

Widening the northbound (River Street) approach to this intersection to extend the left-turn lane should also be pursued. Currently, it supports the existing and proposed lane arrangement except for the continuation of the 5-foot (bike lane) shoulder from Bank Street to River Street. The structure's overall rating is adequate, but the curb-to-curb deck width does not meet the



current requirements. The existing eastern edge of pavement would be maintained in its current location.

Bank Street @ Church Street/Beecher Street

The preferred alternative for this improvement location includes the realignment of Church Street to intersect Beecher Street at a T-intersection along with the narrowing and realignment of the intersection of Beecher Street at Bank Street. This alternative will create a safer condition for both vehicular and pedestrian mobility, will result in the same overall improvement to traffic operations at a much lower cost, and will not require the acquisition of private property. There is an informal roadway/access strip for drop-off and pickup in front of the Russian American Citizen Club. This area is within the public right-of-way but is used almost exclusively by the club and will remain available for limited parking. The additional turning lane on Beecher Street approaching Bank Street will help to reduce delays for motorists turning right due to left-turning vehicles.

Bank Street @ Klarides Village Driveway/Johnson Avenue

The proposed improvements for this area include the termination of Johnson Avenue at Route 67 along with prohibiting left turns from Klarides Village by constructing a modified median. The improvements listed below are primarily intended to improve traffic safety at this intersection:

Johnson Avenue at Bank Street

The preferred alternative offered herein includes the construction of a hammerhead intersection immediately adjacent to the existing residential properties closest to Route 67 that would allow the access of emergency and maintenance vehicles. This plan will require a partial taking of property east of Johnson Avenue for the turnaround area. Elimination of this access point will improve the safety of users at this intersection and provide for a free flow of traffic along Route 67. This option will require Johnson Avenue area residents to seek alternate access to Route 67.

Klarides Village and Bank Street (unsignalized)

The preferred alternative for this side of the intersection is to physically prohibit the current no-left-turn restriction by adding a physical barrier. Vehicles turning left or heading east along Route 67 will be required to drive through the plaza to the existing signalized driveway. Physically prohibiting the ability to turn left will eliminate the safety concerns and the queuing issues at the unsignalized intersection. This design is expected to have minimal to no impacts on rights-of-way and utilities. Stakeholder impacts will be essentially limited to those patrons exiting McDonald's and TD Banknorth and wishing to travel east on Route 67.



Additional Traffic Signalization Improvements

Signalization improvements are also recommended at two intersections as described below.

Bank Street @ Klarides Village

The traffic analysis supports modifying the signal timing at this intersection. Reducing the cycle length from 90 seconds to 60 seconds will maintain overall operations of LOS A and will significantly reduce 95th percentile queues, especially for the eastbound approach (850+ feet to 300 feet).

Bank Street/Old Drive (west)

While a new traffic signal was added as part of the development of the Walgreens site, the analysis has determined that the signal timing needs to be adjusted at Old Drive (west) to accommodate the improvements proposed under this project.

Pedestrian Circulation

An evaluation of pedestrian infrastructure was conducted to identify pedestrian-related issues and connectivity gaps. In general, the study area does not effectively provide for safe pedestrian mobility throughout. While a sidewalk network exists, many areas are in disrepair, crosswalks are not handicap compliant, and gaps exist in many areas making it unsafe for pedestrians to travel from Klarides Village and points west to downtown Seymour.

PRELIMINARY CONSTRUCTION COST OPINION

Johnson Avenue Access Termination	\$52,280
Klarides Plaza Entrance	\$26,785
Church Street/Beecher Street Realignment	
Bank Street (Route 67) – Old Drive to River Street/Franklin Street Intersection	
Southeast Corner of Bank Street/River Street	\$148,235
River Street (SR 313) Widening – including bridge improvements	
, , ,	. ,

Total (after adding inflation to 2019, contingencies, incidentals, etc.) *\$3,970,000

FUNDING 80% FEDERAL / 10% STATE / 10% TOWN

PROJECT SCHEDULE

All dates below are subject to the availability of funding, permit approvals, and right-of-way acquisitions/relocations:

- Completion of Preliminary Engineering Study Phase winter 2015
- Final Design Phase 2016 to 2018
- Construction spring 2019



^{*}Excludes right-of-way acquisition costs, utility relocations, streetscape enhancements, and hazardous materials if any.

COMMENTS AND ADDITIONAL INFORMATION

See correspondence attachments as summarized below.

- Invitation to Stakeholder Meetings on 10/13/15 and 10/15/15
- Public Notice for Public Information Meeting on 10/19/15 (including newspaper proof)
- Deed (Vol. 114, Page 579) and Copy of Plan from project 124-148 submitted by Housatonic Wire Company depicting limits of land ownership around the island at the intersection of Church Street and Beecher Street
- 10/12/15 letter from John J. Borgesano (Russian American Club) to town (w/enclosure)
- 10/15/15 Letter from John J. Borgesano (Russian American Club) to town (w/enclosure)
- 12/2/15 email from Milone & MacBroom, Inc. to Ms. Fatima Silva (#117-#119 Bank Street)

Comments and discussions from the public during the stakeholder meetings, public information, and in correspondence before and within 30 days after October 19, 2015 are summarized below and are organized by location:

General Comments and Concerns

- The public in attendance was generally in favor of the need to perform improvements along Route 67 (Bank Street) to improve traffic operations through the corridor, especially improvements to the traffic signal timings and coordination. Larger regional concerns and questions were raised regarding what long-term planning efforts have been performed or will be performed for Route 67 in Seymour and Oxford and all the way out to Southbury. Concerns were raised about how developments in other towns were affecting traffic in Seymour.
- Residents reported that some of the biggest traffic problems occur during school bus pickup and drop-off times.
- Residents described current driving behavior and patterns that motorists familiar with the
 area use to avoid intersections within the project limits. More specifically, many
 represented that drivers often avoid using the Church Street/Beecher Street intersection to
 access Bank Street and instead use West Street to travel toward Oxford and areas west of
 the project limits.

Bank Street From Old Drive to Franklin Street/River Street (SR 313)

- It was noted that changes to the existing conditions since the start of the study include the new signal improvements and development associated with the construction of Walgreens on the north side of Bank Street, the demolition of the existing buildings on the southwestern corner of the Bank Street/River Street intersection, and new cantilevered sidewalk improvements to the Route 67 Bridge Over Little River (State Project No. 124-167).
- As indicated during the presentation and given the anticipated impacts, full acquisitions are anticipated for the remaining residential and commercial properties along the southern side of Bank Street. The property owners in attendance, which included the owners of Ed's Dry



Cleaners (115 Bank Street) and Chet Sobotka, the trustee for the estate of Richard Sobotka (111 Bank Street), expressed a general understanding of the purpose of the improvements and related impacts but requested an accelerated rights-of-way acquisition process. With the knowledge that the project would create these impacts, the owners expressed concern about the costs and ongoing efforts that are needed to maintain, rent, use, or sell these properties for an undetermined time until the acquisitions will occur. These concerns were echoed by Fatima Silva (117-119 Bank Street) during a phone conversation with MMI after the public information meeting. An approximate schedule for when the rights-of-way process may begin was offered by representatives of MMI and NVCOG, and the residents were informed that the CTDOT would initiate the formal rights-of-way acquisition and relocation discussions after the formal design of the project commences. Any decisions regarding accelerated acquisitions would need to be made by CTDOT and would be dependent on the availability of state and federal funding.

- The public was in support of the geometric and lane improvements proposed at the intersection, including the elimination of the parallel parking spaces on the northeastern corner of the intersection.
- The additional length of the northbound River Street left-turn lane was acknowledged as an important improvement to the intersection. It was stated that while signs are posted on portions of West Street prohibiting use by trucks both car and truck drivers often use West Street to avoid the River Street/Bank Street/Franklin Street intersection in order to access Route 67 and other areas west of the project limits.

Bank Street @ Church Street/Beecher Street

- Representatives from the Russian American Club (#20 Church Street) submitted correspondence dated 10/12/15 and 10/15/15 expressing concerns about the potential loss of the informal "on-street" parking. This area along their property and adjacent to the traffic island at the intersection of Church Street and Beecher Street has been used by the club for years for parking and deliveries. With no on-site parking for the property due to severe topographic elevation changes, relocation of the parking on site does not seem feasible.
- The club representatives indicated that without a similar number of parking spaces and available loading/delivery area they will not be able to host events at the club and could be put "out of business."
- Representatives of the church indicated that it was their understanding that the area used for parking and the intersection island may be owned by the club. Additional deed and map information was submitted by representatives of the Housatonic Wire Company indicating the island club parking area is likely owned by Housatonic Wire Company. This is information that was not obtained by the CTDOT during its survey and land record research efforts for this project. It was indicated by the Russian American Club and Housatonic Wire Company that in 1994 under state project 124-148 the CTDOT decided not to pursue modifications to the island and parking area due to concerns raised by the club. The next phase of design will include a more detailed rights-of-way analysis including title searches, which will aid in clarifying the private and public ownership limits.



- A request was made by the Russian American Club and other members of the public who use Church Street and Beecher Street to consider improvements closer to Bank Street, including changes to the east radius to accommodate the desire to provide a right- and left-turn lane while limiting the changes to Church Street and Beecher Street. Analysis of this option will need to consider both the vertical and horizontal limitations associated with Church Street and the elevation changes along Allen's Plumbing supply.
- Concern was raised about the newer traffic signal improvements at Old Drive/Rimmon Street west of Church Street, and a question was raised if the western end of Old Drive/Rimmon Street could be shifted to align with Church and Beecher. Residents indicated that given the amount of traffic on Route 67 and the location between two traffic signals left turns from Church/Beecher onto Route 67 are often difficult and likely contribute to the reason vehicles use West Street to bypass this location. However, the ability to realign the intersections is limited by permitting, hydraulic, structural, and cost implications associated with the work that would be required for the existing Route 67 Little River bridge crossings. Those challenges appear to significantly outweigh the traffic improvements the realignment would provide.
- Suggestions were also made to consider converting Beecher Street from one way to two
 way. This would need to be assessed in relation to the on-street parking that is currently
 provided for the residences along the western side of Beecher Street.
- During the next phase of design, adjustments to the preferred alternative can be analyzed in relation to the public comments in order to provide the desired traffic improvements while minimizing the impacts to the current use of the public right-of-way.

Bank Street @ Klarides Village Plaza Driveway/Johnson Avenue

- Paul Lepezzo, a representative for McDonald's, expressed concern about the future ability of delivery trucks, which currently use the unsignalized driveway for access, to use the driveway if the island is installed. It was explained that the intent of the improvements at the driveway and on Route 67 is to provide adequate space for vehicles to turn left into the property but prevent/deter vehicles from turning left out of the property. Left-turning vehicles exiting the site, including trucks, will need to use the existing signalized shopping plaza entrance to the west. The existing on-site parking configuration and proposed island to deter left turns from the plaza can be analyzed during the next phase of design to accommodate the turning movements of delivery vehicles that need to use this entrance. Options such as but not limited to a raised but mountable island may be considered.
- At Johnson Avenue, the preferred alternative was generally accepted. The property owner at the southern end of Johnson Avenue (#20 Old Drive) complained about vehicles that currently use her driveway and property to turn around without permission. The preferred alternative, which includes a turnaround area and limits access to Route 67 to town and emergency vehicles only, would formalize through an easement or partial acquisition the activities that currently occur.

MILONE & MACBROOM

OCTOBER 19, 2015 7:00 PM

ROUTE 67 (BANK STREET) SPOT IMPROVEMENTS - SEYMOUR, CT PRELIMINARY ENGINEERING PHASE - PUBLIC INFORMATION MEETING

MMI Project No. 3211-02

PUBLIC INFORMATION MEETING STATE PROJECT NO. 124-165

203-272-9733 FAX 203-271-1773 203-888-2856 203-535-9797 PHONE mikej@miloneandmacbroom.com paulcarvalhojr@yahoo.com woosterborg@yahoo.com housatonicwire@aol.com EMAIL Jachimowskicci@att.net fstanek@wtsblaw.com jkoerkel@gmail.com djpeck830@att.net chets5@aol.com grud84@att.net eb47@att.net 29 Rimmon Street, Seymour, CT 06483 14031 Monterra Avenue, Fontana, CA 1 Meadow Woods Road, Seymour, CT 481 Oxford Road, Oxford, CT (office) 17 Sacko Drive, Seymour, CT 06483 99 Realty Drive, Cheshire CT 06410 145 Bank Street, Seymour, CT ADDRESS 87 Blackberry Hill, BF 87 Blackberry Hill, BF 20 Church Street 20 Church Street 109 River Street 30 Emma Street 69 West Street 31 Elm Street Milone & MacBroom, Inc. COMPANY E&S E&S Gregory Omelchenko Stanley Jachimowski John Borgesano NAME **Tom Gabianelli** Alex Budzinski Michael Joyce Rich Grudzias Elaine Bariluk David A. Bitso Paul Carvalho Chet Sobotka John Koerkel Fred Stanek **Devid Peck** John Allen

20 Church Street, Seymour, CT midio12@gmail.com	47 Pershing Avenue (20 Church Street) mark.solanch@att.net	18 Carriage Drive cidio12@gmail.com	49 William Street. Seymour, CT		bal 52 Main Street, Seymour, CT	43 Church Street, Seymour, CT	106 West Street, Seymour, CT
20 Church St	47 Pershing /	18 Carriage [49 William St	McDonald's	Michael H. Horbal Land Surveyors & Planners	43 Church St	106 West Str
Michael Díon	Mark Solanch	Cindy Dion	Jack Santore	Paul Lepezzo N	Michael Horbal	Gwyn Sussman	Bill Wareholik

INVITATION

TOWN OF SEYMOUR

BANK STREET (ROUTE 67) SPOT IMPROVEMENTS STATE PROJECT NO. 124-165

PRELIMINARY ENGINEERING STUDY

NEIGHBORHOOD STAKEHOLDER MEETINGS October 13th and October 15th, 2015 6:00 PM to 8:00 PM

The Town of Seymour (Town) and the Naugatuck Valley Council of Governments (NVCOG) have prepared a Preliminary Engineering Study for spot improvements along Bank Street (Route 67) from the Klarides Village shopping center, east to the Naugatuck River Bridge, including improvements to Johnson Avenue.

The Town and NVCOG hereby extend an invitation to the property owners and residents along and adjacent to the project corridor to attend one of two evening "workshop" meetings on October 13th and 15th at Town Hall to review and discuss the project, the improvements and related impacts in more detail with the Town, NVCOG and the engineer. These "workshop" meetings are being held in advance of a more formal public information meeting on October 19, 2015 (see attached Public Notice) when the project will be presented to the general public.

All meetings will be held in the Seymour Town Hall, Norma Drummer Room, 1 First Street, Seymour, Connecticut 06483. All persons interested in this project are encouraged to attend the public information meeting. Additional information from the preliminary engineering study will be provided to the public and residents at this meeting and will be made available on the Town's website.

Anyone interested in obtaining further information or providing input on this project may do so by contacting the Director of Economic Development, Rory Burke at 203-888-2511 or at rburke@seymourct.org

TOWN OF SEYMOUR

PUBLIC NOTICE

BANK STREET (ROUTE 67) SPOT IMPROVEMENTS STATE PROJECT NO. 124-165

PRELIMINARY ENGINEERING STUDY PUBLIC INFORMATION MEETING

The Naugatuck Valley Council of Governments (NVCOG) has prepared a Preliminary Engineering Study for spot improvements along Bank Street (Route 67) from the Klarides Village shopping center east to the Naugatuck River Bridge, in the Town of Seymour. The study includes a preliminary analysis of geometric and traffic signalization improvements along the corridor including but not limited to roadway widening, driveway access management at Klarides Village, realignment of the Bank Street/Church Street/Beecher Street intersection and potential closure of Johnson Avenue to through traffic.

It is the policy of the Town of Seymour, NVCOG and the State of Connecticut Department of Transportation (DOT) to keep persons informed and involved when such projects are undertaken. It is important that the community be informed and provide meaningful input to assist in the project's development. The Town of Seymour will hold a public informational meeting on October 19, 2015 at 6:00 pm in the Seymour Town Hall, Norma Drummer Room, 1 First Street, Seymour, Connecticut 06483. All persons interested in this project are encouraged to attend the public information meeting.

Anyone interested in obtaining further information or providing input on this project may do so by contacting the Director of Economic Development, Fred Messore at 203-463-3008 office or at fmessore@seymourct.org

RepublicanAmerican

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Classified Advertising Proof

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DANA FLACH SEYMOUR, TOWN OF FIRST SELECTMAN'S OFFICE 1 FIRST STREET SEYMOUR, CT 06483 203-888-2511

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Start date: 10/3/2015 | Stop date: 10/3/2015 |

Insertions: 1

Title: Rep-Am.com | Class: L-Legal -Public Notice 019

Start date: 10/3/2015 | Stop date: 10/3/2015 |

Insertions: 1

TOWN OF SEYMOUR
PUBLIC NOTICE
BANK STREET (ROUTE 67) SPOT
IMPROVEMENTS
STATE PROJECT NO. 124-165
PRELIMINARY ENGINEERING STUDY
PUBLIC INFORMATION MEETING

The Naugatuck Valley Council of Governments (NVCOG) has prepared a Preliminary Engineering Study for spot Improvements along Bank Street (Route 67) from the Klarides Village shopping center east to the Naugatuck River Bridge, in the Town of Seymour. The study includes a preliminary analysis of geometric and traffic signalization improvements along the corridor including but not limited to roadway widening, driveway access management at Klarides Village, realignment of the Bank Street/Church Street/Beecher Street Intersection and potential closure of Johnson Avenue to through traffic.

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Anyone interested in obtaining further information or providing input on this project may do so by contacting the Rory Burke, 203-888-2511; rburke@seymourct.org RA-October 3, 2015

Total Order Price: \$141.52

Please call or send an email by 3pm to approve or to make changes. (No call back will result in your ad running as it appears on this proof.)

Advertisements placed on CTJobs.com, AfterCollege.com and Recruitment Networks run for 30 days

Salesperson: Mari-Jayne | Printed on: 10/2/2015

Telephone: 203-574-3636 ext 1165 | Fax: 203-754-0644

October 15, 2015

Mr. Roy Burke, Director if Economic Development Town of Seymour 1 First Street Seymour, Ct.

Re: Bank Street (Route 67) Spot Improvements State Project No. 124-165

Dear Mr. Burke

The Russian American Club located on #20 Church Street, Seymour has reviewed Figure 6 of the Preliminary Engineering Study and submit the following comments:

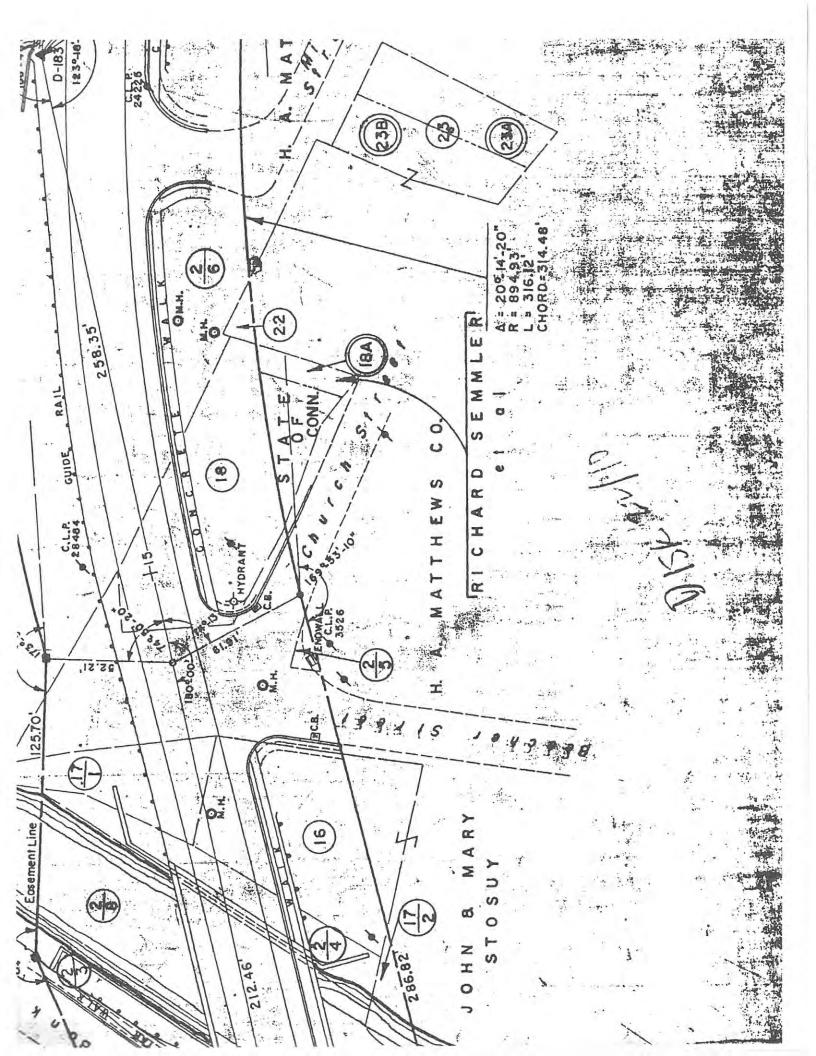
- 1. The Russian American Club has been in business since 1938.
- 2. The Russian American Club has used the front area in question since 1938.
- 3. Without the front area we will be without an area for loading or unloading of goods.
- 4. The 8 parking spaces allow our more senior members easy access to the front of the Club.
- 5. We have donated to the town charities, parades and help out the local fire department with fund raising.
- 6. Without the loading, unloading and parking area, we will be unable to run our business leaving us without funding to donate
- 7. Without the area in question we will basically be out of business.

We the members of the Russian American Club urge the Town to carefully examine the benefits vs what it will do the Russian American Club as an Entity.

Very truly yours John J Borgesano

RAC

Chairman: Building and Grounds



October 12, 2015

Mr. Rory Burke, Director of Economic Development Town of Seymour 1 First Street Seymour, CT 06483

Re: Bank St. (Route 67) Spot Improvements State Project No. 124-165

Dear Mr. Burke:

The Russian American Citizens Club located at # 20 Church Street, Seymour has reviewed Figure 6 of the Preliminary Engineering Study and submit the following comments:

- 1. The Russian American Citizens Club (RA Club) currently has seventy four (74) members who actively support the club and the Town.
- 2. Annually, the Christmas Party, the St. Patrick's Day Party and various parties, birthday, anniversary, wedding, etc. are held in the hall. During these occasions it is not uncommon to have over 100 participants and 40 -50 cars and our parking is extremely limited.
- 3. The existing parking lot at the intersection of Church and Beecher Streets serves two important functions: (a.) to accommodate up to eight parking spaces for club members and their guests and (b.) to provide a loading area for delivery trucks.
- 4. Figure 6 proposed to take much of the parking area to allow Church Street to be revised to intersect with Beecher Street approximately 40 ft. south off the edge of Bank Street

Other than moving Church Street 20 ft. south and taking away much needed parking and loading space for the RA Club what does it do? Is there a high rate of accidents here? We don't think so.

In 1994 the Town undertook State Project No. 124-148 and listened to the concerns of the RA Club and did not take away any of its land or parking.

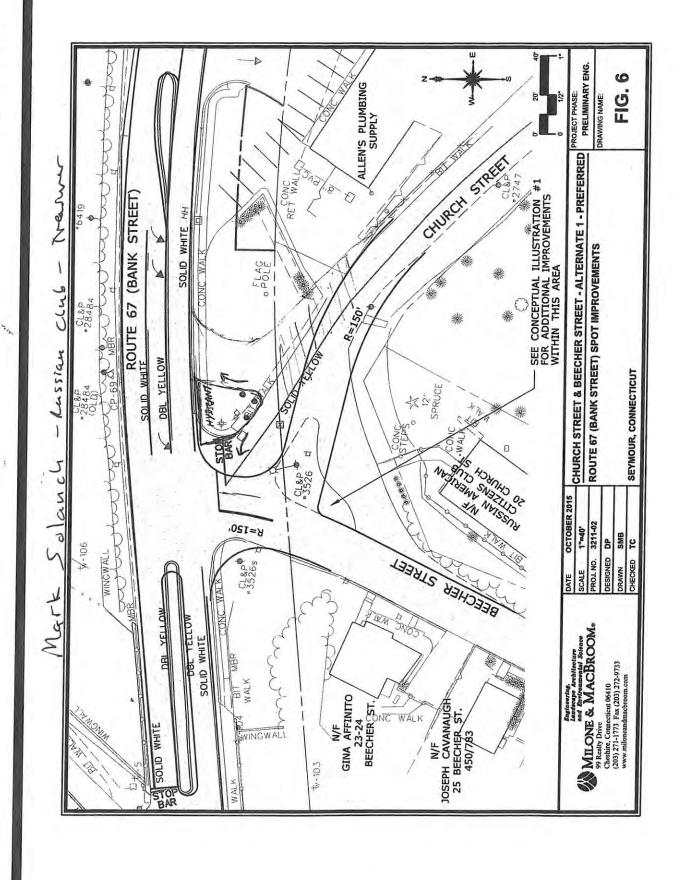
If constructed according to Figure 6, would cars still be able to enter the lot from Beecher St. and exit onto Church Street? If not, then delivery trucks would either have to back into the parking lot or back out of it onto Beecher Street causing a dangerous situation.

We, the RA Club members urge the Town to carefully examine the benefits of the design and eliminate it form the project.

Very truly yours,

7517 Byr

11



VOL 114 PAGE 579

FIFTH PIECE:

Consisting of such rights as The James Swan Company may have had in and to a private road known as Mill Street running Westerly from the Westerly line of the third piece hereinbefore described.

EASTERLY : by the third piece hereinbefore described, 27-1/2 feet;

SOUTHERLY: by land now or formerly of Ida Swan and land now or formerly of State of Connecticut, 274 feet, more or less:

NORTHWESTERLY: by state highway Route No. 67 taking line, 60 feet, more or less; and

NORTHERLY: by other land now or formerly of Ida Swan, 209.27 feet.

Said piece of land being formerly used as a private roadway by The James Swan Company and others.

SIXTH PIECE:

Being a small piece, more or less triangular in shape.

NORTHEASTERLY : by Church Street;

SOUTHERLY : by a drive which runs along land now or formerly

occupied by the Russian-Hall, so-called;

NORTHWESTERLY : by Beecher Street; and

NORTHERLY : by State Highway Route No. 67, the last line being 23 feet, more or less, in length.

Said premises being a portion of the third piece described in the deed from the Estate of Frank H. Beecher recorded in said land records, in Volume 24 on Page 87.

Said piece is subject to such rights as may exist, if any, concerning the placing and maintenance of a pole thereon as set forth in said conveyance from The James Swan Company to The United Electric Light and Water Company above mentioned.

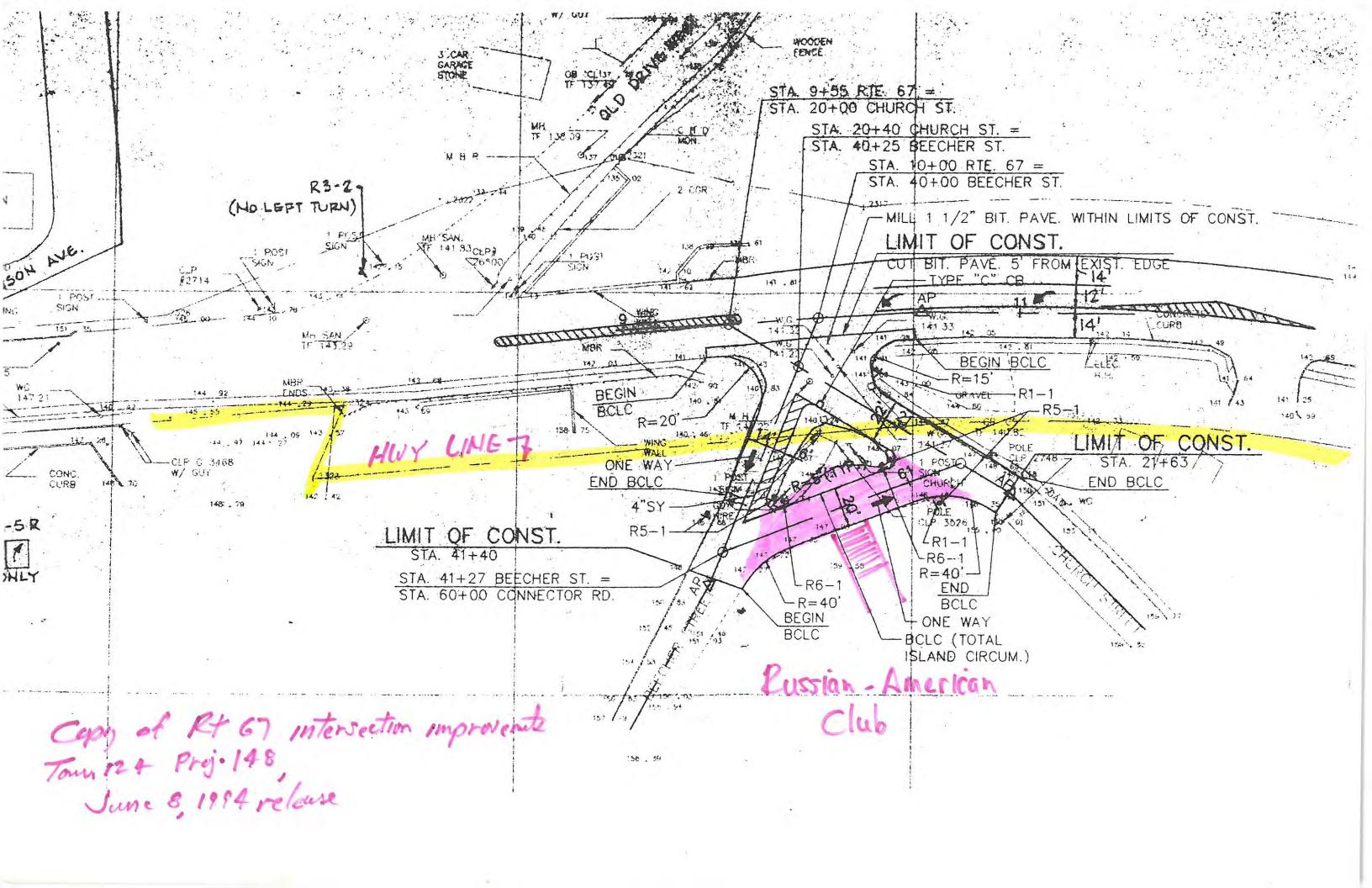
SEVENTH PIECE:

Being a small piece of land largely covered by Little River, lying Southwesterly from the Southwesterly face of the old iron bridge hereinbefore mentioned and extending as far as the Northeasterly face of the dam known as the Beecher Dam, and being a portion of the second piece in said deed from the Estate of Frank H. Beecher recorded in Volume 24 on Page 87.

Commencing at the Southwesterly corner of said old iron bridge which formerly led to Church Street from Bank Street; thence Northwesterly along the Southwesterly side of said bridge, 49 feet, more or less, to Bank Street;

SAMUEL H. D'AMBRUOSO
ATTORNEY AT LAW
ONE THOMPSON PLACE
DERBY, CONNECTIGUT
OS418

JURIS NUMBER



Mike Joyce

From:

Mike Joyce

Sent:

Wednesday, December 02, 2015 8:23 AM

To:

'timasilva@netzero.net'

Subject:

Route 67 - Bank Street - Spot Improvements - Seymour

Attachments:

Final-PIM-brochure.pdf

Ms. Silva,

Please find attached the public information meeting brochure for the Route 67 (Bank street) spot improvements project.

I've also provided a link below which provide more information about the project.

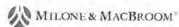
http://nvcogct.org/publication/route-67-preliminary-engineering-study

Please do not hesitate to contact our office with any questions.

Thank you,

Michael J. Joyce, P.E., Associate

Manager of Highway Design



99 Realty Drive / Cheshire, Connecticut 06410 203.271.1773 Ext. 205 / 203.272.9733 (Fax) 860,841.2924 Cell

www.miloneandmacbroom.com



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